

Abrasion Wear Resistance of Precipitation-Hardened Al-Zn-Mg Alloy

Rodinger, Tomislav; Lukšić, Helena; Ćorić, Danko; Rede, Vera

Source / Izvornik: **Materials**, 2024, 17, 1 - 14

Journal article, Accepted version

Rad u časopisu, Završna verzija rukopisa prihvaćena za objavljivanje (postprint)

<https://doi.org/10.3390/ma17102446>

Permanent link / Trajna poveznica: <https://urn.nsk.hr/urn:nbn:hr:235:014979>

Rights / Prava: [Attribution 4.0 International](#)/[Imenovanje 4.0 međunarodna](#)

Download date / Datum preuzimanja: **2024-06-26**

Repository / Repozitorij:

[Repository of Faculty of Mechanical Engineering
and Naval Architecture University of Zagreb](#)



Article

Abrasion Wear Resistance of Precipitation-Hardened Al-Zn-Mg Alloy

Tomislav Rodinger , Helena Lukšić, Danko Ćorić *  and Vera Rede

Department of Materials, Faculty of Mechanical Engineering and Naval Architecture, University of Zagreb, Ivana Lučića 5, 10000 Zagreb, Croatia; tomlav.rodinger@fsb.unizg.hr (T.R.); helena.luksic@fsb.unizg.hr (H.L.); vera.rede@fsb.unizg.hr (V.R.)

* Correspondence: danko.coric@fsb.unizg.hr

Abstract: The heat treatment of aluminum alloys is very important in industries where low weight in combination with high wear resistance, good strength, and hardness are important. However, depending on their chemical composition, aluminum alloys are subjected to different mechanical and thermal treatments to achieve the most favorable properties. In this study, an Al-Zn-Mg alloy was heat-treated including solution annealing at 490 °C for 1 h with subsequent artificial aging at 130, 160, and 190 °C for 1, 5, and 9 h. The hardness (HV1) and abrasive wear resistance with three different abrasive grain sizes were measured for all samples. The highest hardness was measured for the samples artificially aged at 130 °C/5 h, 227 HV1, while the lowest hardness was measured for the samples aged at 190 °C/9 h. The highest and the lowest wear resistance was also observed for the same state, i.e., artificially aged at 130 °C/5 h and 190 °C/9 h, respectively. The critical abrasive grain size was detected for some samples, where a decrease in wear rate was observed with an increase in the abrasive grain size from the medium value to the largest. The Response Surface Methodology (RSM) was applied to demonstrate the influence of the input parameters on the material wear rate.

Keywords: aluminum alloy; precipitation hardening; abrasion; wear rate; critical abrasive grain size



Citation: Rodinger, T.; Lukšić, H.; Ćorić, D.; Rede, V. Abrasion Wear Resistance of Precipitation-Hardened Al-Zn-Mg Alloy. *Materials* **2024**, *17*, 2446. <https://doi.org/10.3390/ma17102446>

Academic Editor: Jordi Sort

Received: 11 April 2024

Revised: 9 May 2024

Accepted: 17 May 2024

Published: 19 May 2024



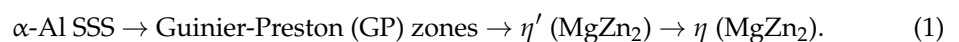
Copyright: © 2024 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<https://creativecommons.org/licenses/by/4.0/>).

1. Introduction

The development of aluminum alloys is very important from the perspective of lightweight engineering, mainly in aeronautical [1,2] and automotive industries [3,4], where it can reduce up to 60% of the mass compared to the steel part it replaces [5,6]. In the case where a high strength–weight ratio is needed, aluminum alloy properties often need to be improved. This can be achieved by alloying with different elements and varying their content, cold working, or heat treatment.

Heat-treatable Al alloys are mostly solution-treated at temperatures above 450 °C to dissolve alloying elements in the aluminum matrix. Solution treatment is followed by quenching to obtain a supersaturated solid solution (SSS) α -Al matrix. Then, the material is aged at room (natural aging) or higher temperature (artificial aging) [7]. The increase in mechanical properties is the result of the formation of precipitates from the SSS α -Al matrix [8].

Al-Zn-Mg alloys are generally characterized by especially large yield strength and ultimate tensile strength (UTS) after aging [9]. In these alloys, magnesium is the main alloying element that increases the strength by forming the η (MgZn₂) intermetallic phase, which has a high solid solubility in the Al matrix [10], according to the following equation [11,12]:



GP zones are nanosized coherent pre-precipitates (or solute clusters) that are formed during natural aging and in the early stages of artificial aging from which the semi-coherent transitional metastable η' phase, and eventually, the final incoherent equilibrium η phase

nucleate and grow [12]. With the increase in Mg content, the volume fraction of η precipitates increases, which improves the yield strength, but lowers toughness and promotes the probability of intergranular fracture [13,14]. Zinc promotes the nucleation and growth of precipitates during age hardening, which also increases the strength of the alloy and shortens the heat treatment time [10].

A very large number of problems in industry are caused by abrasive wear, and it is assumed that this results in costs in the amount of 1–4% of the gross national product of industrialized countries [15]. To minimize these costs, great efforts are being made to investigate how to increase the wear resistance of various structural materials. In the scope of the 7xxx group of Al alloys, Reis et al. [16] investigated abrasive wear of two different Al-Zn-Mg alloys and proposed a correlation between wear, hardness, and UTS, where wear decreases with the increase in hardness and UTS. Focusing on different Zn and Mg content in Al-Zn-Mg alloys, Pruthvi and Shenoy [17] investigated wear properties after solution and retrogression re-aging heat treatment. Their study concludes that the wear rate decreases, i.e., the material is more wear-resistant with the increase in Zn content and re-aging duration. With the increase in aging temperature and time, the size of the precipitates increases, but this does not mean that the wear rate increases. Yildirim et al. [18] found that 7075 Al alloy has the lowest wear rate when aged at 120 °C for 24 h, even though $MgZn_2$ precipitates continue to grow with higher temperatures or longer aging times.

The influence of the abrasive grain size on the wear rate has already been studied, and in some cases, the critical abrasive grain size (CAGS) has been noticed, as shown in Figure 1. In those studies, three main types of curves have been described: after reaching the CAGS, the wear rate continues to increase but with lower intensity (curve 1), or the wear rate remains unchanged (curve 2), while in some cases it even starts to decrease (curve 3) [19].

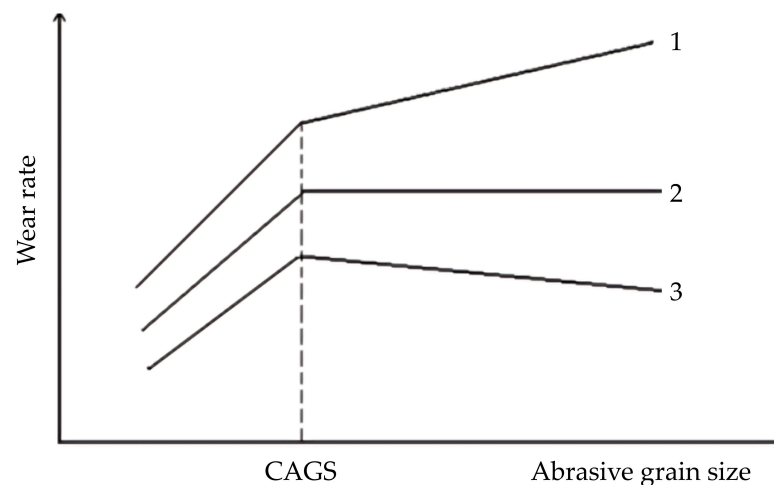


Figure 1. Types of wear rate curves depending on the abrasive grain size where CAGS has been noticed [19].

This phenomenon of the change in wear rate trend with varying abrasive size can be observed in various metallic [19–22] and non-metallic [23] materials.

By the application of the design of experiment (DOE) method and statistical analysis of the obtained results, the optimal regime of artificial aging which resulted in the lowest wear rate was determined. The experimental results were statistically studied by the analysis of variance (ANOVA) and represented by the Response Surface Methodology (RSM). These methods are widely accepted in different areas, especially in materials research. They were used to optimize the sintering parameters of alumina ceramics [24], to evaluate boride surface layer thickness on steel [25], tool wear during the machining of Al/SiC composite [26], but also to compare the aging parameters of Al alloys on their yield strength, hardness [27], and thermal properties [28].

This research aimed to investigate the influence of different artificial aging parameters (temperature and time) of Al-Zn-Mg alloy on its abrasive wear rate by different abrasive grain sizes concerning the hardness achieved.

2. Materials and Methods

For the intended experiments, an Al alloy was used whose chemical composition is shown in Table 1. The analysis of the chemical composition was performed with an optical emission spectrometer GDS 850A (Leco, Saint Joseph, MI, USA). Based on the chemical composition, it is clear that this is an Al-Zn-Mg alloy. These aluminum alloys from the 7xxx series are known for their high specific strength, stiffness, processability, and weldability, and are widely used in the aerospace, rail traffic, and civil infrastructure industries [29–31].

Table 1. Chemical composition of Al alloy.

| Element, wt. % | | | | | | | | | | |
|----------------|------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| Zn | Mg | Fe | Mn | Si | Zr | Cu | Sb | Ti | Cr | Al |
| 7.68 | 3.54 | 0.222 | 0.206 | 0.151 | 0.109 | 0.044 | 0.042 | 0.039 | 0.013 | bal. |

A total of two groups with 10 samples each were cut from the Al rod using a band saw with water cooling. The samples were cylindrical with a diameter of 20 mm and a height of 10 mm, as shown in Figure 2.



Figure 2. Two groups of Al samples.

After analyzing the chemical composition, the density of the material was measured which was later used for the determination of volume loss (ΔV) and wear rate ($\dot{\omega}$) during abrasion tests. Density was measured by the Archimedes principle with an analytical balance type JP703C (Mettler Toledo, Zürich, Switzerland). The mean density value of the three measurements was $\rho = 2.7857 \text{ g/cm}^3$.

After determining the chemical composition, the heat treatment temperatures were chosen. Precipitation hardening was carried out in an electric furnace (Over, Sveta Nedelja, Croatia). Solution treatment of all samples was performed at $490 \text{ }^\circ\text{C}$ for 1 h, followed by quenching in water. The temperature for solution treatment was determined based on the ternary Al-Zn-Mg diagram available in [32]. One sample (ST-Q) was only solution-treated and quenched in water, without subsequent artificial aging, while the other samples were subjected to artificial aging. The temperatures and times of artificial aging were varied on three levels ($130, 160, \text{ and } 190 \text{ }^\circ\text{C}$; 1, 5, and 9 h, respectively) as shown in Table 2. Two samples were subjected to the same aging regime.

After heat treatment, the samples were tested for wear resistance with the Taber abraser device (Taber Industries, North Tonawanda, NY, USA) with a rotating abrasive disc of 125 mm in diameter. The wear test samples were cut into the shape of a four-sided prism with dimensions of approximately $5 \text{ mm} \times 5 \text{ mm} \times 10 \text{ mm}$, and the cross-sectional area of $5 \text{ mm} \times 5 \text{ mm}$ was worn. From each cylindrical sample, one prism for the wear test was cut so that each thermal state was tested on two samples. During the test, the

samples were pressed against a rotating disk with mounted sandpaper with a constant force of 4.91 N. The disk rotated at a speed of 60 rpm, and the relative tangential speed of the sample was 0.251 m/s. Figure 3 schematically shows the testing technique. For the abrasion wear resistance, three types of Al_2O_3 sandpaper with different grain sizes were used, as shown in Table 3. The samples were tested for 100 s on each sandpaper, which corresponds to an approximate wear length of 25 m. The wear tests were carried out with sandpapers in the following order: P600, P280, and P180. All the samples were in about the same initial condition before each test, i.e., they had similar roughness of the test surface. The tested surface of the samples was polished with sandpaper P800 before each wear test to ensure approximately the same surface quality. This eliminated the stress concentrator effect determined by the degree of roughness, which can ultimately be reflected in the hardness values of the surface layer. Before and after the wear test, the sample mass was measured on a precision balance with a resolution of 0.0001 g (type B5C 1000, Mettler Toledo, Zurich, Switzerland) to determine the mass loss (Δm) and convert it to volume loss (ΔV). Also, before each wear test, the cross-sectional area of the worn surface was measured to calculate the abrasive wear rate ($\dot{\omega}$) as a ratio of the volume loss and wear surface.

Table 2. Artificial aging temperatures and times.

| State | Artificial Aging Temperature, °C | Artificial Aging Time, h |
|-------|----------------------------------|--------------------------|
| ST-Q | -/- | -/- |
| 130/1 | 130 | 1 |
| 130/5 | 130 | 5 |
| 130/9 | 130 | 9 |
| 160/1 | 160 | 1 |
| 160/5 | 160 | 5 |
| 160/9 | 160 | 9 |
| 190/1 | 190 | 1 |
| 190/5 | 190 | 5 |
| 190/9 | 190 | 9 |

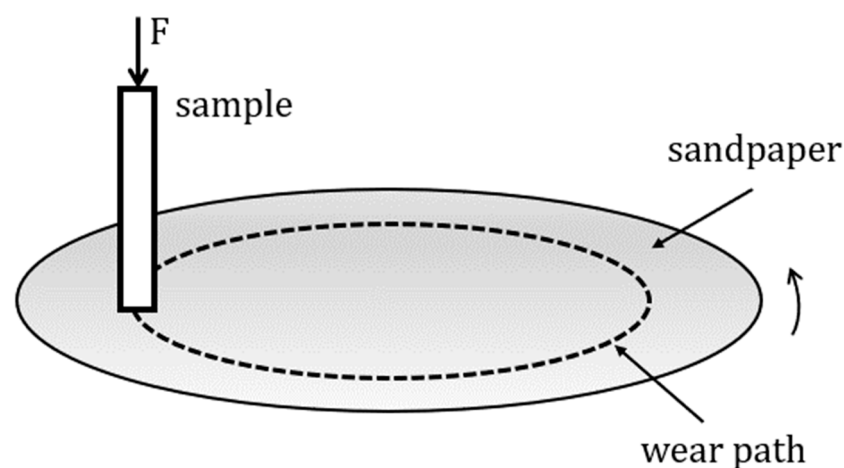


Figure 3. Schematic representation of tests with the Taber abraser device [33].

Table 3. Average abrasive grain sizes of used sandpapers.

| ISO/FEPA Grit Designation | Average Abrasive Grain Size, μm |
|---------------------------|--|
| P600 | 25.8 |
| P280 | 52.2 |
| P180 | 82.0 |

The hardness of the samples was measured after metallographic preparation, which included mounting, planar grinding, rough polishing, and final polishing, as shown in Figure 4. The grinding of the samples was carried out in four steps using sandpapers of different sizes of SiC abrasive particles on the device Phoenix Alpha (Buehler, Lake Bluff, IL, USA). The sandpapers were used in the following order: P600, P1200, P2500, and P4000. The grinding plate rotated at a speed of 300 rpm. During the grinding process, the samples were cooled with water to avoid possible microstructural transformations due to heating. After that, a two-step polishing process was carried out on the same device. As a polishing base, a cloth with diamond paste applied was used. The cooling agent during the polishing was a lubricant. In the first step, diamond paste with a 3 μm average diameter of abrasive particles was used, while a polishing liquid with a 0.03 μm average diameter of abrasive particles was used in the second polishing step. During the polishing, the plate rotated at a speed of 150 rpm. The hardness measurement was carried out by the standard Vickers method with the Indentec device (ZwickRoell, Ulm, Germany), applying an indentation load of 9.81 N (HV1). Ten hardness measurements were performed on each sample and the mean value was calculated.

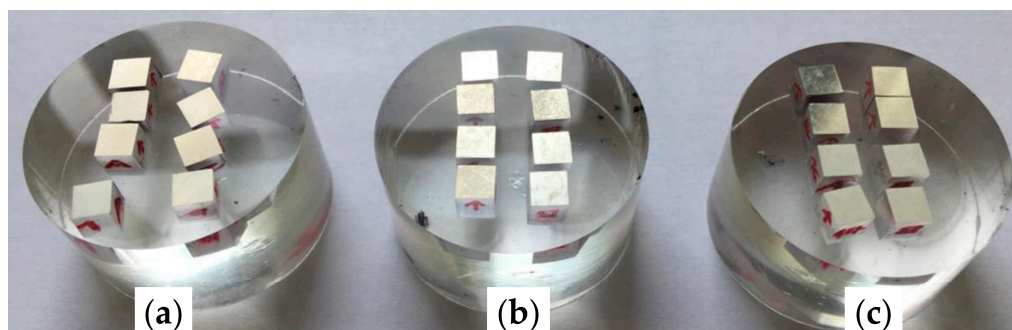


Figure 4. Metallographically prepared samples aged at (a) 130 °C; (b) 160 °C; (c) 190 °C.

For the applicability of the Response Surface Methodology (RSM) based on the obtained data, the results were also processed statistically. For the design of experiment (DOE) and analysis of the obtained results, Design-Expert 13.0.5 software (Stat-Ease, Minneapolis, MN, USA) was used. DOE had three independent variables: artificial aging temperature (A), artificial aging time (B), and average abrasive grain size (C) with three levels of variations: low (−1), center (0), and high (+1), as shown in Table 4. As the real average abrasive grain size for sandpaper quality P280 is not exactly the in the middle of grain sizes for P600 and P180, but it is very close, the center level for abrasive grain size was set as 53.9 μm , which is the average value of the largest and the smallest abrasive grains used.

Table 4. Design of experiment.

| Symbol | Factor | Level | | |
|--------|------------------------------------|-------|------|------|
| | | −1 | 0 | +1 |
| A | Artificial aging temperature, °C | 130 | 160 | 190 |
| B | Artificial aging time, h | 1 | 5 | 9 |
| C | Abrasive grain size, μm | 25.8 | 53.9 | 82.0 |

3. Results and Discussion

Table 5 shows the mean values of mass loss (with standard deviations) and the total average wear rates after abrasion with different sandpaper qualities. The abrasion was tested by three different grits of sandpaper (P600, P280, and P180) for 100 grinding cycles. The samples aged at 130 °C for 5 h showed the lowest total wear rate (the highest wear resistance), and the samples aged at 190 °C for 5 and 9 h had the highest total wear rates (the lowest wear resistance). In Figure 5, the wear rate is represented as a function of the abrasive grain size for each state.

Table 5. Mass losses and total wear rates of samples abraded with different sandpapers.

| State | Mass Loss (Δm), g | | | Total | Total Wear Rate ($\dot{\omega}$), mm ³ /mm ² |
|-------|-----------------------------|-----------------|-----------------|--------|--|
| | P600 | P280 | P180 | | |
| ST-Q | 0.0017 ± 0.0005 | 0.0035 ± 0.0011 | 0.0038 ± 0.0023 | 0.0090 | 0.1256939 |
| 130/1 | 0.0008 ± 0.0002 | 0.0021 ± 0.0005 | 0.0029 ± 0.0003 | 0.0058 | 0.0767269 |
| 130/5 | 0.0007 ± 0.0001 | 0.0025 ± 0.0019 | 0.0017 ± 0.0001 | 0.0049 | 0.0659601 |
| 130/9 | 0.0011 ± 0.0001 | 0.0021 ± 0.0007 | 0.0039 ± 0.0014 | 0.0071 | 0.0942676 |
| 160/1 | 0.0011 ± 0.0003 | 0.0025 ± 0.0013 | 0.0040 ± 0.0012 | 0.0076 | 0.1008957 |
| 160/5 | 0.0012 ± 0.0002 | 0.0023 ± 0.0008 | 0.0023 ± 0.0004 | 0.0058 | 0.0774652 |
| 160/9 | 0.0008 ± 0.0002 | 0.0023 ± 0.0011 | 0.0037 ± 0.0010 | 0.0068 | 0.0899557 |
| 190/1 | 0.0011 ± 0.0001 | 0.0025 ± 0.0014 | 0.0024 ± 0.0010 | 0.0060 | 0.0810531 |
| 190/5 | 0.0020 ± 0.0008 | 0.0033 ± 0.0003 | 0.0045 ± 0.0006 | 0.0098 | 0.1319191 |
| 190/9 | 0.0018 ± 0.0000 | 0.0043 ± 0.0002 | 0.0035 ± 0.0001 | 0.0096 | 0.1312447 |

For some thermal states, the wear rate increases linearly with increasing abrasive grain size (130/1, 160/1, 160/9, and 190/5) or even exponentially (130/9), and remains approximately constant for the last two abrasive sizes (160/5 and 190/1), or begins to decrease (130/5 and 190/9). The phenomenon of critical abrasive grain size is visible for the states ST-Q, 130/5, 130/9, 160/5, 190/1, and 190/9, while at other states (130/1, 160/1, 160/9, and 190/5) it is not observed.

Given that wear resistance is closely related to hardness, the hardness of the samples was measured by the standard Vickers hardness method HV1 ten times for each sample. For the samples that were only solution-treated and quenched in water (ST-Q) without subsequent artificial aging, the average hardness value was 173 ± 6.21 HV1. The lowest hardness value (165 ± 9.48 HV1) was measured on the samples that underwent heat treatment at a temperature of 190 °C for 9 h, while the highest hardness value (227 ± 9.57 HV1) was measured on the samples artificially aged at a temperature of 130 °C for 5 h. The Vickers hardness, as a function of the aging time, for the temperatures of 130, 160, and 190 °C is shown in Figure 6.

The wear rate as a linear function of hardness for the abrasive grain sizes 25.8, 52.2, and 82.0 μm which correspond to the sandpaper qualities P600, P280, and P180 is shown in Figure 7. It is visible that the abrasive grain size affects the correlation coefficient value which is very indicative. For the smallest abrasive grain size of 25.8 μm (sandpaper P600), the correlation coefficient is 0.7909, which indicates a very good correlation between the observed values, as shown in Figure 7a. When testing wear resistance by the P280 sandpaper (the abrasive grain size of 52.2 μm), the correlation coefficient is significantly larger (0.8579), which similarly indicates a very strong correlation between the wear rate and hardness, as shown in Figure 7b. For the largest abrasive grain size of 82 μm (sandpaper P180), the linear regression analysis shows a rather low correlation coefficient of 0.2628, which indicates that only 26.28% of the wear rate variation can explain the linear dependence on hardness, as shown in Figure 7c. From Figure 7, it can be observed that the slope of all three linear functions is negative, which indicates that the wear rate will decrease as the hardness value increases. The highest slope of the linear function was noticed for the abrasive grain size 52.2 μm (sandpaper quality P280), which indicates a greater change in the wear rate compared to other grain sizes. In addition, the smallest slope of the linear function was for the abrasive grain size 25.8 μm (sandpaper quality P600), which indicates the smallest rate of abrasion resistance change with varying hardness.

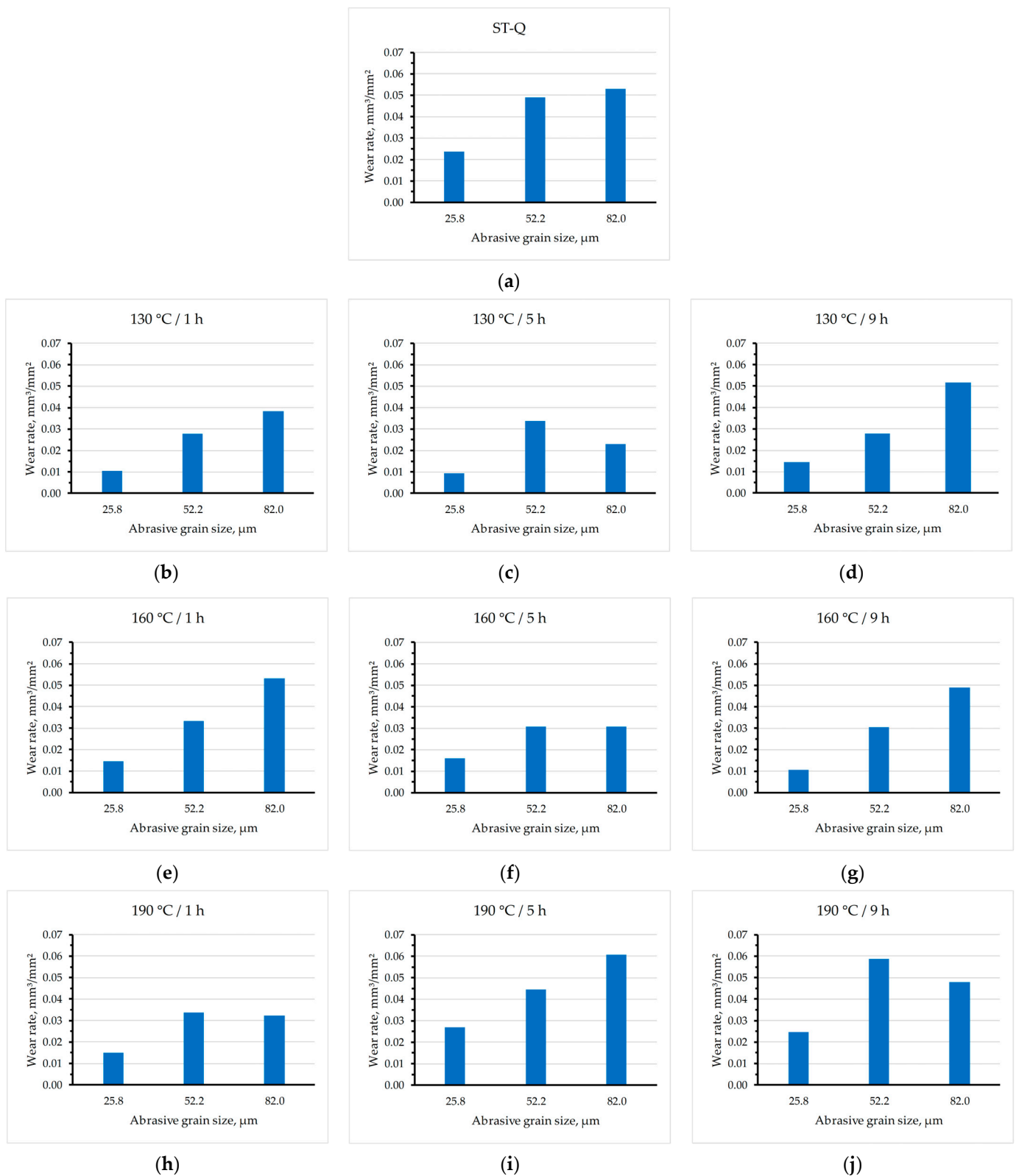


Figure 5. Wear rate of states: (a) ST-Q; (b) 130/1; (c) 130/5; (d) 130/9; (e) 160/1; (f) 160/5; (g) 160/9; (h) 190/1; (i) 190/5; (j) 190/9; abraded with different abrasive grain sizes.

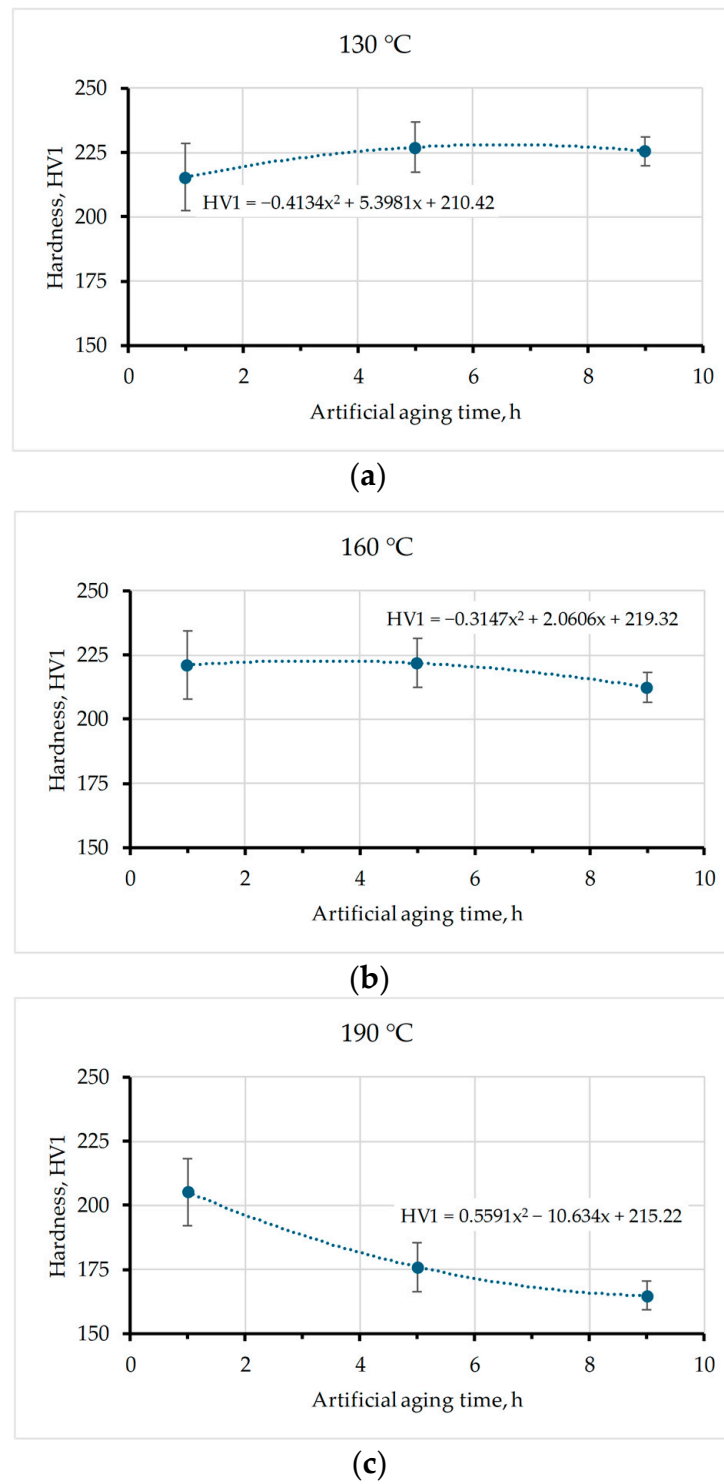
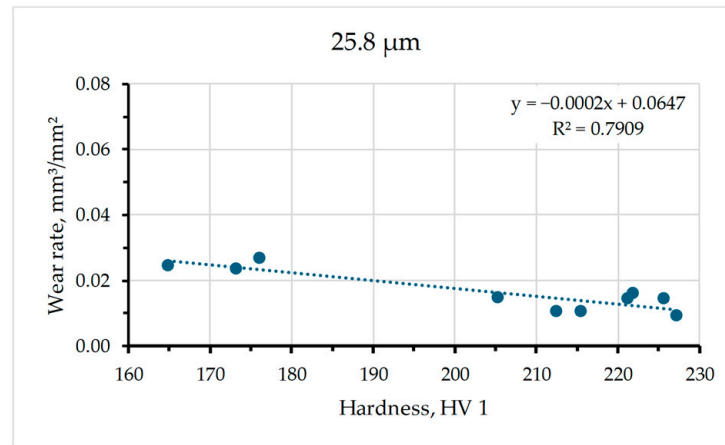
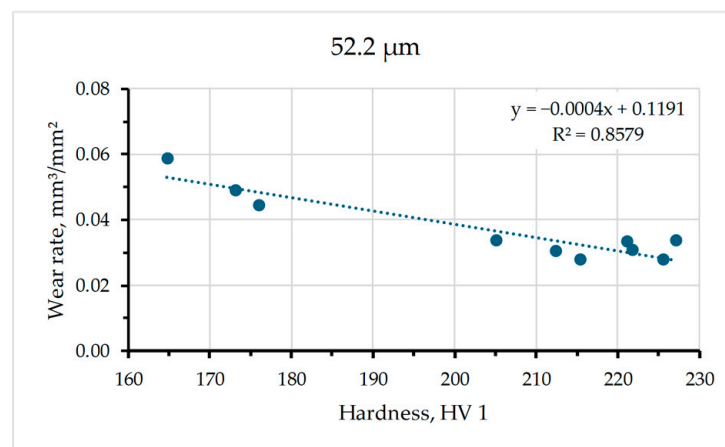


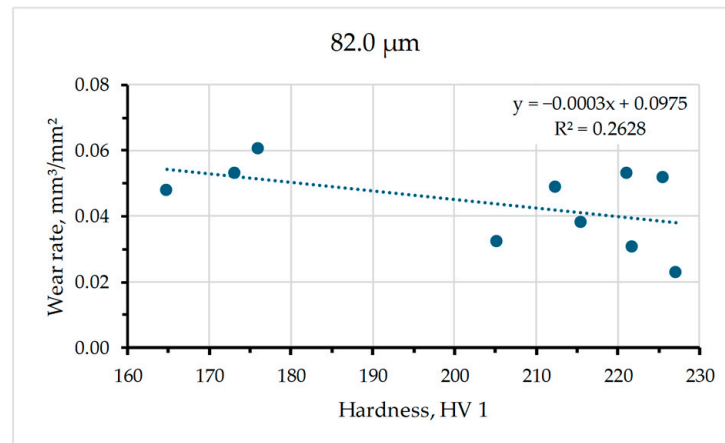
Figure 6. Hardness as a function of aging time, for temperatures: (a) 130 °C; (b) 160 °C; (c) 190 °C.



(a)



(b)



(c)

Figure 7. Wear rate as a function of hardness, for average abrasive grain size of (a) 25.8 μm (P600); (b) 52.2 μm (P280); (c) 82.0 μm (P180).

The combinations of factors that were used for the design of experiment method and the measured wear values are shown in Table 6. The Face-Centered central composite design (CCF) was used for the test, where the value $\alpha = 1$ (star points are at the center of each face of the factorial space). For response 1, the mass loss (Δm) after the test was weighted. For response 2, the wear rate ($\dot{\omega}$), the volume loss ΔV , calculated as a ratio of

Δm and the measured density (2.7857 g/cm³), was divided by the cross-sectional area of the sample.

Table 6. Combinations of factors and the results.

| Factor A | Factor B | Factor C | Response 1 | Response 2 |
|----------------------------|--------------------------|-------------------------|----------------|---|
| Artificial Aging Temp., °C | Artificial Aging Time, h | Abrasive Grain Size, µm | Δm , g | $\dot{\omega}$, mm ³ /mm ² |
| 130 | 1 | 25.8 | 0.0008 | 0.0105830 |
| 130 | 1 | 82.0 | 0.0029 | 0.0383635 |
| 130 | 5 | 53.9 | 0.0025 | 0.0336531 |
| 130 | 9 | 25.8 | 0.0011 | 0.0146048 |
| 130 | 9 | 82.0 | 0.0039 | 0.0517808 |
| 160 | 1 | 53.9 | 0.0025 | 0.0331894 |
| 160 | 5 | 25.8 | 0.0012 | 0.0160273 |
| 160 | 5 | 53.9 | 0.0023 | 0.0307189 |
| 160 | 5 | 82.0 | 0.0023 | 0.0307189 |
| 160 | 9 | 53.9 | 0.0023 | 0.0304262 |
| 190 | 1 | 25.8 | 0.0011 | 0.0148597 |
| 190 | 1 | 82.0 | 0.0024 | 0.0324213 |
| 190 | 5 | 53.9 | 0.0033 | 0.0444217 |
| 190 | 9 | 25.8 | 0.0018 | 0.0246084 |
| 190 | 9 | 82.0 | 0.0035 | 0.0478496 |

Since all three responses are related, the analysis of variance (ANOVA) and model graphs are presented for the final response only, the wear rate. For the measured and calculated results, the modified quadratic model was found to be the most suitable. Based on the ANOVA analysis, the suggested modified quadratic model of wear rate is as follows:

$$\dot{\omega} = 0.152859 - 0.002328 \cdot A + 0.000996 \cdot B + 0.001654 \cdot C + 0.00000743188 \cdot A^2 - 0.000011 \cdot C^2, \quad (2)$$

where

- $\dot{\omega}$ —wear rate, mm³/mm²,
- A—aging temperature, °C;
- B—aging time, h;
- C—abrasive grain size, µm.

Other combinations of factors including AB, AC, BC, and B² were not included in the model because the ANOVA pointed out that these combinations were not significant. The results of the ANOVA for this modified quadratic model of wear rate, which does not include insignificant variables, are presented in Table 7.

Since the F-value of the model is 12.25, it implies that the model is significant and there is only a 0.08% chance (p -value = 0.0008) that this large F-value could occur due to noise. Even though factor A has a large p -value, it is included in the model to support hierarchy. The coefficient of determination (R^2) is relatively close to the value of 1, which suggests that this model describes the obtained results quite well. The predicted R^2 of 0.6353 is in reasonable agreement with the adjusted R^2 of 0.8008.

Figures 8 and 9 show 3D graphical presentations of the combined effects of all input parameters on the wear rate of the precipitation-hardened Al-Zn-Mg alloy. Figure 8 shows the influence of aging temperature and time for various abrasive grain sizes (sandpaper qualities), while Figure 9 presents the effect of average abrasive grain size and aging temperature.

Table 7. ANOVA for modified quadratic model of wear rate (SS—Sum of Squares, DF—Degrees of Freedom, and MS—Mean Square).

| Source | SS | DF | MS | F-Value | p-Value |
|---------------------------------|--------|----|--------|--------------------------|---------|
| Model | 0.0019 | 5 | 0.0004 | 12.25 | 0.0008 |
| A: Artificial aging temperature | 0.0000 | 1 | 0.0000 | 0.7465 | 0.4100 |
| B: Artificial aging time | 0.0002 | 1 | 0.0002 | 5.15 | 0.0494 |
| C: Abrasive grain size | 0.0015 | 1 | 0.0015 | 47.03 | <0.0001 |
| A ² | 0.0001 | 1 | 0.0001 | 4.06 | 0.0747 |
| C ² | 0.0002 | 1 | 0.0002 | 7.31 | 0.0242 |
| Residual | 0.0003 | 9 | 0.0000 | | |
| Cor Total | 0.0022 | 14 | | | |
| Standard deviation | 0.0056 | | | R ² | 0.8719 |
| Mean | 0.0303 | | | Adjusted R ² | 0.8008 |
| Coefficient of variation, % | 18.34 | | | Predicted R ² | 0.6353 |
| | | | | Adeq. Precision | 10.3284 |

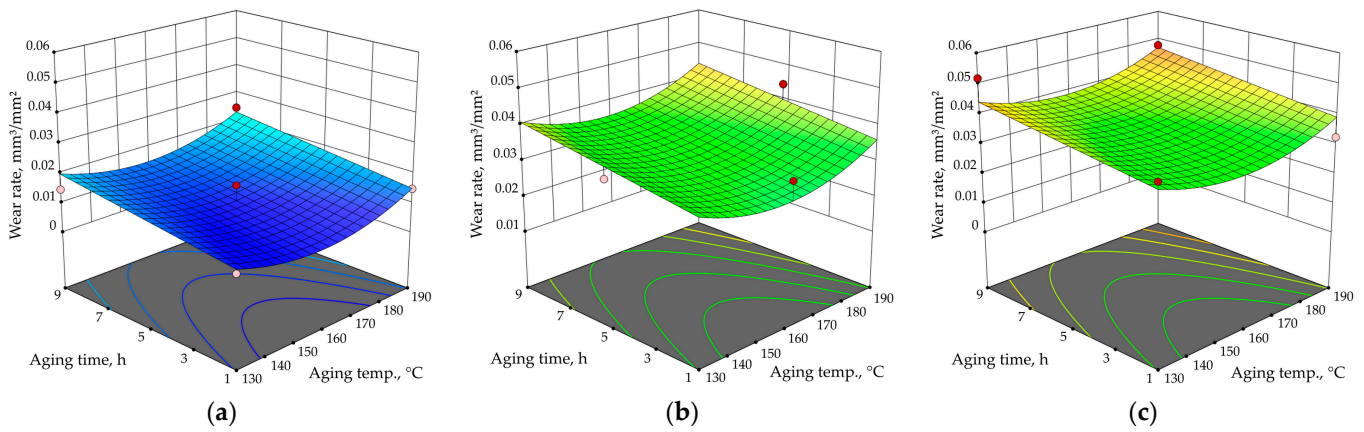


Figure 8. The effect of aging time and temperature on wear rate for average abrasive grain size of (a) 25.8 μm (P600); (b) 52.2 μm (P280); (c) 82.0 μm (P180).

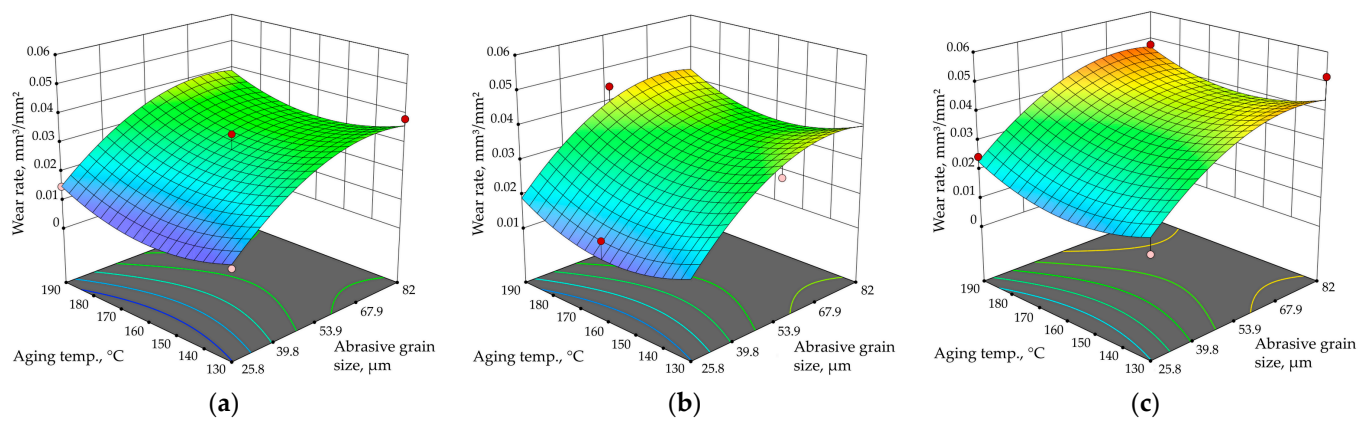


Figure 9. The effect of abrasive grain size and aging temperature on wear rate for aging time of (a) 1 h; (b) 5 h; (c) 9 h.

From Figures 8 and 9, it is obvious that abrasive grain size has the largest influence on the wear rate of strengthened Al-Zn-Mg alloy; while using sandpaper with a larger abrasive grain size, the wear rate generally increases. On the other hand, the artificial aging time does not have a large influence on the abrasion resistance, but this may be the result of the limitation of the central composite design, as it excludes some of the experiment points.

For example, artificially aged samples with the lowest and the highest wear rate (state 130/5 abraded with the finest sandpaper, $\dot{\omega} = 0.0094 \text{ mm}^3/\text{mm}^2$ and state 190/5 abraded with the roughest sandpaper, $\dot{\omega} = 0.0605 \text{ mm}^3/\text{mm}^2$, respectively) are not included in the CCF. Based solely on the results obtained from the CCF, it appears that the sample artificially aged at 130 °C for 1 h and worn with the smallest abrasive size of 25.8 μm has the lowest wear rate ($\dot{\omega} = 0.0105 \text{ mm}^3/\text{mm}^2$). This value is quite close to the actual lowest value for the examined thermal states. In addition, according to the CCF results, the highest wear rate would be for the sample artificially aged at 130 °C for 9 h and abraded with the roughest abrasive size of 82.0 μm ($\dot{\omega} = 0.0517 \text{ mm}^3/\text{mm}^2$), which is not that close to the actual maximum wear rate of $0.0605 \text{ mm}^3/\text{mm}^2$ measured for state 190/5.

4. Conclusions

In this study, the influence of different aging parameters (temperature and time) of Al-Zn-Mg alloy on its resistance to abrasive wear and hardness was investigated. On all the samples, solution treatment was performed at the same parameters (490 °C for 1 h with quenching in water), while the temperature and time of artificial aging were varied (130, 160, and 190 °C; 1, 5, and 9 h, respectively). Based on the results of wear resistance tests and hardness analysis, the following conclusions can be drawn:

- i. Artificial aging parameters (temperature and time) affect resistance to abrasion wear. It was found that aging the material at a temperature of 130 °C for 5 h induces the least wear for both the smallest (25.8 μm) and the largest abrasive grain size (82.0 μm) resulting in the lowest total wear rate (the highest wear resistance). On the other hand, the highest wear for all tested abrasive sizes, and thus the greatest total wear rate (the lowest wear resistance), was recorded when the material was artificially aged at 190 °C for 5 and 9 h.
- ii. In some samples, there is a phenomenon known as critical abrasive grain size. This implies that after a certain abrasive grain size, the wear intensity changes, whereby the wear rate continues to increase with the increase in abrasive size, but faster or slower (130/9, ST-Q), remains approximately the same (160/5, 190/1) or even decreases (130/5, 190/9). For the samples of other thermal states (130/1, 160/1, 160/9, and 190/5), the phenomenon of critical abrasive grain size was not visible. More different abrasive particle sizes are required to accurately determine the critical abrasive grain size.
- iii. The hardness results indicated that the Al-Zn-Mg alloy subjected to aging generally showed increased hardness. The hardness values for different thermal states ranged from 165 HV1 to 227 HV1. The sample that was artificially aged at a temperature of 190 °C for 9 h showed the lowest hardness ($165 \pm 9.48 \text{ HV1}$) which correlates with its very intense wear. On the other hand, the samples aged at 130 °C for 5 h had the highest hardness ($227 \pm 9.57 \text{ HV1}$) which is also consistent with the results of abrasion and the least intense total wear.
- iv. Furthermore, it should be noted that the size of the abrasive grain highly affects the relation between wear rate and hardness.

Author Contributions: Conceptualization, D.Ć. and V.R.; methodology, D.Ć. and V.R.; software, T.R. and H.L.; validation, D.Ć. and V.R.; formal analysis, T.R. and H.L.; investigation, T.R. and H.L.; resources, D.Ć. and V.R.; data curation, T.R. and H.L.; writing—original draft preparation, T.R. and H.L.; writing—review and editing, T.R., H.L., D.Ć. and V.R.; visualization, T.R. and H.L.; supervision, D.Ć. and V.R.; funding acquisition, D.Ć. All authors have read and agreed to the published version of the manuscript.

Funding: This research received no external funding.

Data Availability Statement: The data presented in this study are available upon request from the corresponding author.

Conflicts of Interest: The authors declare no conflicts of interest.

References

1. Zhou, B.; Liu, B.; Zhang, S. The Advancement of 7XXX Series Aluminum Alloys for Aircraft Structures: A Review. *Metals* **2021**, *11*, 718. [\[CrossRef\]](#)
2. Dursun, T.; Soutis, C. Recent Developments in Advanced Aircraft Aluminium Alloys. *Mater. Des.* **2014**, *56*, 862–871. [\[CrossRef\]](#)
3. Ma, P.; Liu, C.; Chen, Q.; Wang, Q.; Zhan, L.; Li, J. Natural-Ageing-Enhanced Precipitation Near Grain Boundaries in High-Strength Aluminum Alloy. *J. Mater. Sci. Technol.* **2020**, *46*, 107–113. [\[CrossRef\]](#)
4. Yang, Z.; Zheng, X.; Liang, Z.; Banhart, J. Refreshing Industrially Processed 6xxx Series Aluminum Alloys After Prolonged Natural Aging. *Adv. Eng. Mater.* **2023**, *25*, 2301102. [\[CrossRef\]](#)
5. Hirsch, J. Recent Development in Aluminium for Automotive Applications. *Trans. Nonferrous Met. Soc. China* **2014**, *24*, 1995–2002. [\[CrossRef\]](#)
6. Luo, A.A. Recent Advances in Light Metals and Manufacturing for Automotive Applications. *CIM J.* **2021**, *12*, 79–87. [\[CrossRef\]](#)
7. Sha, G.; Marceau, R.K.W.; Ringer, S.P. Precipitation and Solute Clustering in Aluminium: Advanced Characterisation Techniques. In *Fundamentals of Aluminium Metallurgy: Production, Processing and Applications*; Lumley, R., Ed.; Woodhead Publishing: Cambridge, UK, 2011; pp. 345–366.
8. Lendvai, J. Precipitation and Strengthening in Aluminium Alloys. *Mater. Sci. Forum* **1996**, *217–222*, 43–56. [\[CrossRef\]](#)
9. Kenesei, P.; Horváth, G.; Bernstorff, S.; Ungár, T.; Lendvai, J. Early Stages of Nucleation and Growth of Guinier-Preston Zones in Al-Zn-Mg and Al-Zn-Mg-Cu Alloys. *Int. J. Mater. Res.* **2006**, *97*, 315–320. [\[CrossRef\]](#)
10. Wang, J.; Li, F. Research Status and Prospective Properties of the Al-Zn-Mg-Cu Series Aluminum Alloys. *Metals* **2023**, *13*, 1329. [\[CrossRef\]](#)
11. Xu, X.; Zheng, J.; Li, Z.; Luo, R.; Chen, B. Precipitation in an Al-Zn-Mg-Cu Alloy During Isothermal Aging: Atomic-Scale HAADF-STEM Investigation. *Mater. Sci. Eng. A* **2017**, *691*, 60–70. [\[CrossRef\]](#)
12. Zhao, Y.H.; Liao, X.Z.; Jin, Z.; Valiev, R.Z.; Zhu, Y.T. Microstructures and Mechanical Properties of Ultrafine Grained 7075 Al Alloy Processed by ECAP and Their Evolutions During Annealing. *Acta Mater.* **2004**, *52*, 4589–4599. [\[CrossRef\]](#)
13. Li, H.; Cao, F.; Guo, S.; Jia, Y.; Zhang, D.; Liu, Z.; Wang, P.; Scudino, S.; Sun, J. Effects of Mg and Cu on Microstructures and Properties of Spray-Deposited Al-Zn-Mg-Cu Alloys. *J. Alloys Compd.* **2017**, *719*, 89–96. [\[CrossRef\]](#)
14. Shu, W.X.; Hou, L.G.; Zhang, C.; Zhang, F.; Liu, J.C.; Liu, J.T.; Zhuang, L.Z.; Zhang, J.S. Tailored Mg and Cu Contents Affecting the Microstructures and Mechanical Properties of High-Strength Al-Zn-Mg-Cu Alloys. *Mater. Sci. Eng. A* **2016**, *657*, 269–283. [\[CrossRef\]](#)
15. Swain, B.; Bhuyan, S.; Behera, R.; Sanjeeb Mohapatra, S.; Behera, A. Wear: A Serious Problem in Industry. In *Tribology in Materials and Manufacturing—Wear, Friction and Lubrication*; Patnaik, A., Singh, T., Kukshal, V., Eds.; IntechOpen: Rijeka, Croatia, 2021; pp. 1–20. [\[CrossRef\]](#)
16. Reis, B.P.; Lopes, M.M.; Garcia, A.; dos Santos, C.A. The Correlation of Microstructure Features, Dry Sliding Wear Behavior, Hardness and Tensile Properties of Al-2wt%Mg-Zn Alloys. *J. Alloys Compd.* **2018**, *764*, 267–278. [\[CrossRef\]](#)
17. Pruthvi, H.M.; Ghanashyam Shenoy, H. Effect of Wear Parameter on Al-Zn Alloy on Wear Rate by Using Taguchi's Technique. *Mater. Today Proc.* **2022**, *59*, 79–84. [\[CrossRef\]](#)
18. Yildirim, M.; Özyürek, D.; Gürü, M. The Effects of Precipitate Size on the Hardness and Wear Behaviors of Aged 7075 Aluminum Alloys Produced by Powder Metallurgy Route. *Arab. J. Sci. Eng.* **2016**, *41*, 4273–4281. [\[CrossRef\]](#)
19. Coronado, J.J.; Sinatora, A. Effect of Abrasive Size on Wear of Metallic Materials and Its Relationship with Microchips Morphology and Wear Micromechanisms: Part 1. *Wear* **2011**, *271*, 1794–1803. [\[CrossRef\]](#)
20. Sin, H.; Saka, N.; Suh, N.P. Abrasive Wear Mechanisms and the Grit Size Effect. *Wear* **1979**, *55*, 163–190. [\[CrossRef\]](#)
21. Coronado, J.J.; Sinatora, A. Effect of Abrasive Size on Wear of Metallic Materials and Its Relationship with Microchips Morphology and Wear Micromechanisms: Part 2. *Wear* **2011**, *271*, 1804–1812. [\[CrossRef\]](#)
22. Coronado, J.J. Effect of Abrasive Size on Wear. In *Abrasion Resistance of Materials*; Adamiak, M., Ed.; InTech: Rijeka, Croatia, 2012; pp. 167–184. [\[CrossRef\]](#)
23. Essert, S.; Rede, V.; Barišić, J. Effect of Abrasive Grain Size on the Abrasion Volume Loss of Subfossil and Recent Oak Wood in Three Characteristic Sections. *Materials* **2023**, *16*, 432. [\[CrossRef\]](#)
24. Landek, D.; Ćurković, L.; Gabelica, I.; Kerolli Mustafa, M.; Žmak, I. Optimization of Sintering Process of Alumina Ceramics Using Response Surface Methodology. *Sustainability* **2021**, *13*, 6739. [\[CrossRef\]](#)
25. Milinović, A.; Stojišić, J.; Kladarić, I.; Matijević, B. Evaluation of Boride Layers on C70W2 Steel Using a New Approach to Characterization of Boride Layers. *Materials* **2022**, *15*, 3891. [\[CrossRef\]](#)
26. Laghari, R.A.; Li, J.; Xie, Z.; Wang, S. Modeling and Optimization of Tool Wear and Surface Roughness in Turning of Al/SiCp Using Response Surface Methodology. *3D Res.* **2018**, *9*, 46. [\[CrossRef\]](#)
27. Dehghani, K.; Nekahi, A.; Mirzaie, M.A.M. Using Response Surface Methodology to Optimize the Strain Aging Response of AA5052. *Mater. Sci. Eng. A* **2010**, *527*, 7442–7451. [\[CrossRef\]](#)
28. Vishwakarma, D.K.; Kumar, N.; Padap, A.K. Modelling and Optimization of Aging Parameters for Thermal Properties of Al 6082 Alloy Using Response Surface Methodology. *Mater. Res. Express* **2017**, *4*, 046502. [\[CrossRef\]](#)
29. He, H.; Wu, X.; Sun, C.; Li, L. Grain Structure and Precipitate Variations in 7003-T6 Aluminum Alloys Associated with High Strain Rate Deformation. *Mater. Sci. Eng. A* **2019**, *745*, 429–439. [\[CrossRef\]](#)

30. Zhao, Y.; Yang, Z.; Domblesky, J.P.; Han, J.; Li, Z.; Liu, X. Investigation of Through Thickness Microstructure and Mechanical Properties in Friction Stir Welded 7N01 Aluminum Alloy Plate. *Mater. Sci. Eng. A* **2019**, *760*, 316–327. [[CrossRef](#)]
31. Azarniya, A.; Taheri, A.K.; Taheri, K.K. Recent Advances in Ageing of 7xxx Series Aluminum Alloys: A Physical Metallurgy Perspective. *J. Alloys Compd.* **2019**, *781*, 945–983. [[CrossRef](#)]
32. Raghavan, V. Al-Mg-Zn (Aluminum-Magnesium-Zinc). *J. Phase Equilibria Diffus.* **2007**, *28*, 203–208. [[CrossRef](#)]
33. Rede, V.; Essert, S.; Šokčević, Z. Effects of Microstructural Orientation on the Abrasive Wear Resistance of Subfossil Elm Wood in Three Orthogonal Planes. *Wear* **2017**, *380–381*, 1–5. [[CrossRef](#)]

Disclaimer/Publisher’s Note: The statements, opinions and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions or products referred to in the content.