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## Article

# Alternative Fuels for the Marine Sector and Their Applicability for Purse Seiners in a Life-Cycle Framework

Maja Perčić, Nikola Vladimir <sup>\*</sup>, Marija Koričan , Ivana Jovanović and Tatjana Haramina

Faculty of Mechanical Engineering and Naval Architecture, University of Zagreb, Ivana Lučića 5, 10002 Zagreb, Croatia; maja.percic@fsb.hr (M.P.); marija.korican@fsb.hr (M.K.); ivana.jovanovic@fsb.hr (I.J.); tatjana.haramina@fsb.hr (T.H.)

\* Correspondence: nikola.vladimir@fsb.hr

**Abstract:** Fossil fuel combustion is a major source of Greenhouse Gases (GHGs), which cause global warming. To prevent further increases in anthropogenic GHGs, the global community needs to take action in each segment of the economy, including the shipping sector. Among different measures for reducing shipping emissions, the most promising one is the replacement of conventional marine fuels with alternatives. According to the International Maritime Organisation's regulations, ships engaged in international shipping need to reduce their annual emissions by at least 50% by 2050. However, this does not apply to fishing vessels, which are highly dependent on fossil fuels and greatly contribute to air pollution. This paper investigates the environmental footprint of a fishing vessel (purse seiner) through the implementation of various alternative fuels. Within the research, Life-Cycle Assessments (LCAs) and Life-Cycle Cost Assessments (LCCAs) are performed, resulting in life-cycle emissions and lifetime costs for each alternative, which are then compared to a diesel-powered ship (baseline scenario). The comparison, based on environmental and economic criteria, highlighted methanol as the most suitable alternative for the purse seiner, as its use onboard resulted in 22.4% lower GHGs and 23.3% lower costs in comparison to a diesel-powered ship.

**Keywords:** fishing sector; purse seiner; alternative fuels; LCA; LCCA; decarbonisation



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## 1. Introduction

### 1.1. Research Background

Over the last few decades, extensive use of fossil fuels has resulted in increased Greenhouse Gases (GHGs) in the atmosphere. These emissions refer to the emissions of carbon dioxide (CO<sub>2</sub>), methane (CH<sub>4</sub>), nitrous oxide (N<sub>2</sub>O), and fluorinated gases at low concentrations. They form a thin layer in the atmosphere that prevents solar irradiation from being reflected from the Earth's surface to space, and as a result, it causes the greenhouse effect, which leads to global warming [1]. The Glasgow Climate Pact of 2021 is the most recent climate agreement, which reaffirmed the Paris Agreement's ambitions for limiting the global average temperature increase to 1.5 °C above pre-industrial levels [2,3]. To combat the global warming problem, some urgent measures need to be taken, including a sharp GHG reduction in all sectors of the economy, including the shipping sector.

According to the Fourth GHG Study of the International Maritime Organisation (IMO), the share of shipping GHG emissions in global anthropogenic GHG emissions in 2018 was 2.89%, an increase of 9.6% compared to 2012. Without any emission reduction measures, the study predicts a great increase in emissions by the end of 2050 [4]. Due to that, the IMO set the Initial Strategy for GHG reduction, which is in line with the Paris Agreement temperature goals. The strategy has three levels of ambitions: reduction in carbon intensity (CO<sub>2</sub> emissions per transport work) through the implementation of further phases of the Energy Efficiency Design Index (EEDI) for new ships; reduction in carbon intensity by at least 40% by 2030 and 70% by 2050; and reduction in total annual GHGs by at least

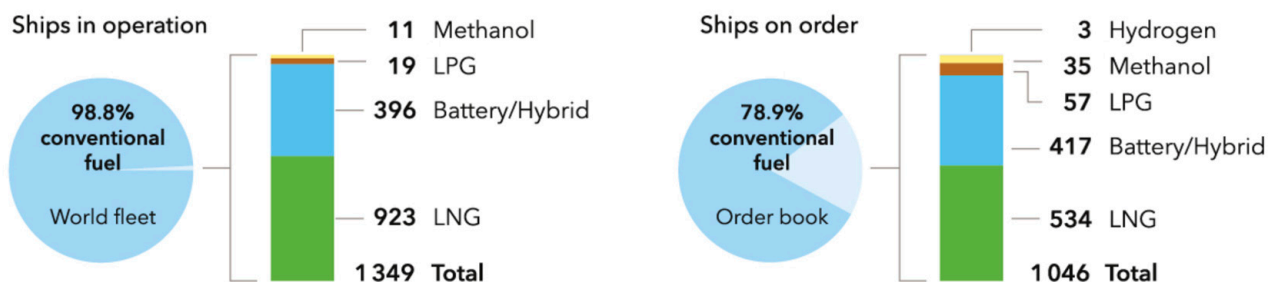
50%, compared to 2008 levels [5]. In order to achieve IMO decarbonisation goals, the strategy indicated measures with the following timelines: short-term (2018–2023), mid-term (2023–2030), and long-term (2030–) measures. Short-term measures represent the start of reducing shipping emissions with national plans, a tighter EEDI, the Ship Energy Efficiency Management Plan (SEEMP), speed reduction, etc. [6]. As a mid-term measure, the IMO has adopted new ship energy efficiency regulations for existing ships, i.e., the Energy Efficiency Existing Ship Index (EEXI) and Carbon Intensity Indicator (CII), which entered into force on the 1st of January 2023. The EEXI is a technical measure of energy efficiency related to the design of a ship, while the CII represents the operational measure of energy efficiency embedded into the SEEMP, and it measures CO<sub>2</sub> emissions per transport work for cargo, cruise, and ro-ro passenger ships over 5000 gross tonnage (GT). Like its predecessor, the EEDI, the EEXI should be applied for all ships above 400 GT, and their calculated, i.e., attained EEXI needs to be less than or equal to the required EEXI [7,8].

The mid-term measure whose implementation represents an incentive towards zero-carbon technologies is the inclusion of the shipping sector in the Emission Trading System (ETS). As of 2024, commercial cargo and passenger ships of above 5000 GT operating in the European Union will be required to purchase carbon allowances for each ton of released CO<sub>2</sub> emission [9].

### 1.2. Review of Alternative Fuels for the Marine Sector

Around 5.5% of GT of ships in operation and one-third of order ships will be powered by alternative marine fuels [10] (Figure 1).

#### NUMBER OF SHIPS



#### IN % OF GROSS TONNAGE

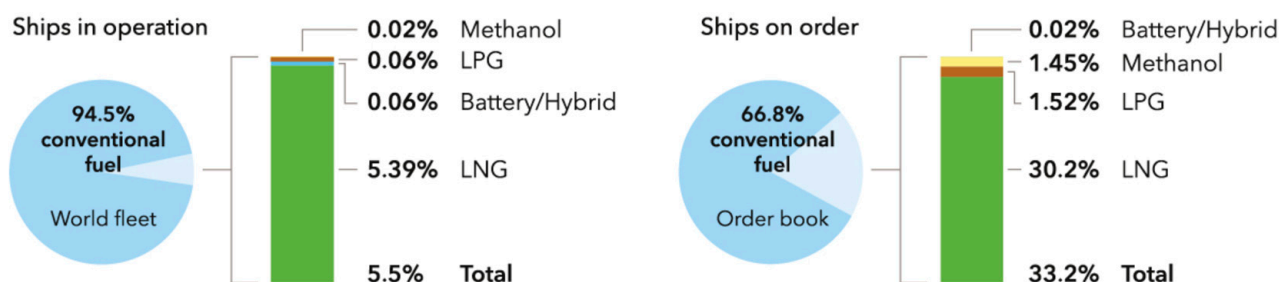


Figure 1. Alternative marine fuel uptake in 2022 [10] (reproduced from [10] with permission of DNV, 2022).

Alternative marine fuels widely investigated within the science community can be divided into low-carbon, carbon-neutral, and zero-carbon fuels (Figure 2).

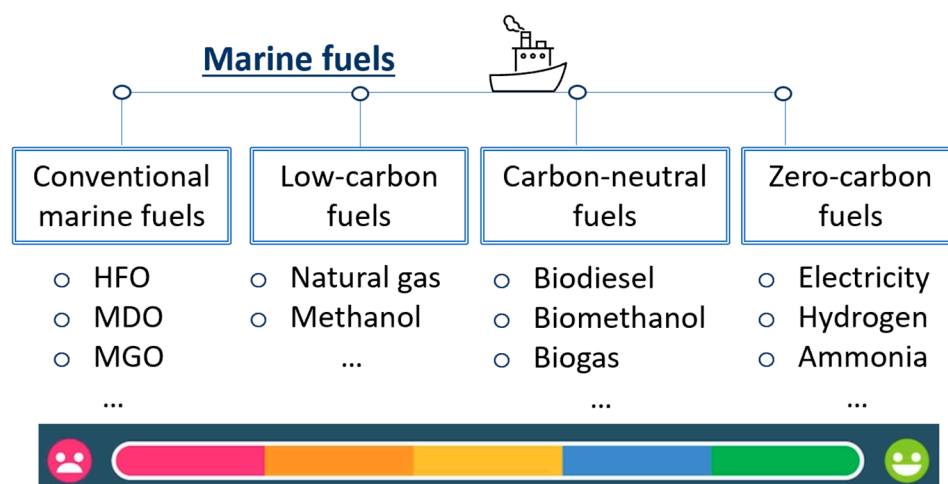


Figure 2. Fuels for maritime purposes.

### 1.2.1. Low-Carbon Fuels

Low-carbon fuels refer to cleaner fossil fuels with a lower carbon content than conventional marine fuels [11]. Natural gas is a low-carbon fuel with no sulphur and nitrogen atoms compared to conventional marine fuels. Due to that, it can easily be used for operation in Emission Control Areas (ECAs) [12,13]. For transportation purposes, it can be used in compressed form, i.e., Compressed Natural Gas (CNG), or in liquefied form, i.e., Liquefied Natural Gas (LNG) [14]. Natural gas is liquefied by cooling to  $-163\text{ }^{\circ}\text{C}$  to make handling easier, occupying 600 times less volume than in its gaseous state [15]. Nowadays, most LNG-powered ships are powered by dual-fuel engines, which ensure a smooth transition from fuel to fuel without affecting performance and efficiency [16]. However, current investment costs, undeveloped infrastructure, and safety issues are major limitations for its use as an alternative fuel [17–19].

Liquefied Petroleum Gas (LPG) is also considered an alternative to conventional marine fuels due to its high energy density and clean burning properties [20]. According to Yeo et al. [21], LPG is suitable for small to medium-sized domestic ships, such as fishing vessels. Moreover, as onboard LPG energy systems are compatible with ammonia-fuelled systems with only minor modifications, LPG can serve as a transitional fuel for zero-emission shipping with ammonia [22].

Another low-carbon fuel already used in the shipping sector is methanol. Due to its liquid state, methanol can be used in existing diesel infrastructure with minor modifications [23]. Many studies investigated methanol as a marine fuel and concluded that its use reduces harmful emissions [24–27]. Its major drawback is energy density, which is more than 50% lower than the energy density of conventional fuels [28]. However, methanol is still a suitable alternative fuel for the shipping sector, and nowadays, it is being used onboard ferries, cruisers, tankers, etc. [29].

Dimethyl-ether (DME), a clean-burning liquid fuel of high density, is produced through methanol dehydration. Since its physical properties are similar to LPG, DME can be used in LPG infrastructure and dual-fuel engines intended for LPG [30,31]. When combusted, it results in low  $\text{CO}_2$  and  $\text{NO}_x$  emissions, while  $\text{SO}_x$  and PM are not emitted [32].

### 1.2.2. Carbon-Neutral Fuels

Carbon-neutral (or climate-neutral) fuels refer to biofuels due to the general opinion that  $\text{CO}_2$  emissions released during biofuel combustion will be absorbed by new biomass further used for biofuel production. In this manner, combustion-related  $\text{CO}_2$  emissions are not considered in the environmental footprint of a biofuel [33]. The first generation of biofuels refers to biofuels produced from edible biomass (e.g., corn, rapeseed, soybean, sugar cane, etc.), while the second generation represents biofuels derived from inedible

biomass (e.g., poplar, switchgrass, corn stover, organic waste, etc.). The third and fourth generations of biofuels refer to fuel produced from microalgae and genetically modified microalgae [34].

Gilbert et al. [35] showed that using biofuels as marine fuels reduces GHGs by 57–59% compared to conventional marine fuels. However, their wider use onboard ships faces limitations such as availability, high cost, and sustainability of fuels [36]. Like its fossil counterpart (LNG), Liquefied Biogas (LBG) has been identified as a potential alternative fuel for the shipping sector. The transition from using LNG as ship fuel to LBG does not require additional equipment or cost. Since combustion-based CO<sub>2</sub> emissions are not considered, LBG is more environmentally friendly than LNG [37]. The most common biofuel that is being investigated as a marine fuel is biodiesel, which is mainly produced from edible biomass by the transesterification process [34]. Its use onboard has been investigated in many studies [38,39], but it is not a pure fuel. It is limited to blends with diesel (usually 80–95% of diesel and 5–20% of biodiesel) due to poor cold flow properties, which can result in damaging power systems, and limited storage stability [40–42].

### 1.2.3. Zero-Carbon Fuels

Zero-carbon fuels are fuels whose use does not result in CO<sub>2</sub> emissions. These fuels represent promising measures for ship decarbonisation and reaching the IMO's 2050 goal [42].

The electrification of ships represents a game changer for the decarbonisation of the shipping industry. There are three types of electrified ships, i.e., plug-in hybrid ships, hybrid ships, and all-electric ships. Both plug-in hybrid ships and hybrid ships include diesel engines and batteries, while all-electric ships refer to the sole use of batteries for ship power [43]. The main drawbacks of full electrification are limitations regarding battery capacity, degradation and weight, investment costs, charging infrastructure at the docks, and sailing distance [44–46]. Different types of batteries are available for maritime purposes. Perčić et al. [47] investigated three batteries (lithium-ion (Li-ion), nickel-metal hydride, and lead batteries) for use in ferries. Li-ion batteries were highlighted as the most environmentally friendly and cost-effective option. With further development of battery technology, i.e., metal–air batteries [48], the full electrification of ships that operate in the open sea could be feasible.

Hydrogen use onboard ships also achieves zero-emission shipping. Based on its cleanliness, i.e., the sources used for its production, hydrogen can be classified by different colours (grey, brown, blue, yellow, pink, green, etc.). However, hydrogen is still primarily produced from natural gas by steam reforming (known as grey hydrogen) [49]. Due to its low volumetric energy density, hydrogen is difficult to store. Often stored in its liquid form, hydrogen evaporates due to heat leakage into the cryogenic tank, known as boil-off gas, which represents a drawback of liquid hydrogen storage [50]. Due to the fast kinetics of electrochemical reactions and its only by-product being water, hydrogen represents the most appropriate fuel for fuel cells. There are different types of fuel cells that are classified based on their operating temperature: low-temperature fuel cells (~80 °C), intermediate-temperature fuel cells (~200 °C), and high-temperature fuel cells (650–1000 °C) [51]. The application of fuel cells onboard usually refers to satisfying auxiliary power needs [52,53]. However, their use for propulsion is entering a new phase, starting with the first ferry fully powered by fuel cells fuelled with liquid hydrogen which has been in operation in Norway since March 2023 [54].

Hydrogen can also be used in an Internal Combustion Engine (ICE), which is less expensive to produce, has a longer lifetime, and does not require fuel purification before use (which is required for low-temperature fuel cells) [55]. However, its use in ICEs encounters several challenges, e.g., potentially high combustion temperatures, which lead to high NO<sub>x</sub> emissions [56].

Ammonia is a hydrogen-rich fuel whose storage onboard ships is easier than that of hydrogen. It is the second most produced chemical in the world, used mainly as a fertiliser.

Its use on board (in ICEs or fuel cells) does not result in CO<sub>2</sub> and SO<sub>x</sub> emissions, while NO<sub>x</sub> emissions can be eliminated with the proper catalyst. Its main drawbacks are toxicity (for humans and marine life) and corrosiveness, low energy density, and infrastructure, which should be expanded to cover the maritime sector [42].

#### 1.2.4. Electro-Fuels

Electro-fuels are synthetic fuels produced with electricity by combining hydrogen and carbon atoms, either from CO<sub>2</sub> captured from industrial processes through carbon capture and utilisation or direct intake from the atmosphere, known as direct air capture. They can be divided into non-carbon-based e-fuels, like hydrogen and ammonia (belonging to zero-carbon fuels), and carbon-based e-fuels, such as e-methanol, e-methane, etc. (belonging to carbon-neutral fuels) [42,57]. Generally, e-fuels are more expensive than their fossil counterparts, and due to that, subsidies are necessary for their production and use, as well as funding future pilot projects regarding e-fuels.

#### 1.2.5. Comparison of Fuels

Some properties of conventional and alternative marine fuels are presented in Table 1.

**Table 1.** Comparison of different marine fuels [58–61].

	Diesel	LNG	LPG	Methanol	DME	Hydrogen	Ammonia
LHV (MJ/kg)	42.5	46–50.2	46.3	20	28.8	120	18.6
Density (kg/m <sup>3</sup> )	833–881	450	500.5	798	667	0.0838	682.3
Carbon content (%)	>85	75	82.6	38	52	0	0
Flashpoint (°C)	52–96	–136	470	11	235	-	132
Boiling point (°C)	163–399	–160	–42	64.5	–25	–253	–33
Cetane rating	>40	0	-	<5	<55	-	-

Besides the qualitative indicators shown in Table 1, environmental and economic analyses are crucial for the decision-making process, i.e., choosing the appropriate alternative fuel for a particular ship that operates in a specific area. Perčić et al. [62] performed a Life-Cycle Assessment (LCA) and Life-Cycle Cost Assessment (LCCA) of different marine fuels and indicated that among the considered alternatives, fully electrified ships are the most environmentally friendly and cost-efficient alternative to diesel power systems installed on ro-ro passenger ships.

Recent studies on alternative fuels in the marine sector are presented in Table 2. Ha et al. [22] performed an LCA of Heavy Fuel Oil (HFO), LNG, LPG, and methanol as marine fuels onboard a Korean bulk carrier. The study indicated that LPG has the lowest GHG emissions, but the country of import significantly affects overall emissions. Similar research was conducted by Spoof-Tuomi and Niemi [63], who investigated an LCA comparison of Marine Diesel Oil (MDO), LNG, and LBG onboard ro-ro passenger ships. The results showed that the most environmentally friendly option is LBG, whose implementation in the shipping sector would be difficult to achieve without any subsidies. Jeong and Yun [64] explored the cost-effectiveness of Low-Sulphur Fuel Oil (LSFO), LNG, and ammonia onboard container ships. Along with capital, investment, and operational costs, carbon cost was also included in the analysis. The study revealed the introduction of carbon allowances into the shipping sector would not be sufficient to replace conventional fuel with ammonia. However, such a tax policy would increase the chance of LNG being more profitable than LSFO.

**Table 2.** Recent studies on alternative fuels in the shipping sector.

Year	Studies	Coverage		Scope
		Fuels	Test Case	
2023	Jeong and Yun [64]	LSFO; LNG; ammonia	container ship	Economic analysis
	Kim et al. [20]	Diesel; gasoline; LPG; bio-LPG	small fishing vessel	LCA
	Ha et al. [22]	HFO; LNG; LPG; methanol	bulk carrier	LCA
2022	Chen and Lam [65]	Diesel; hydrogen	tugboat	LCA
	Huang et al. [66]	MGO; LNG; methanol; ammonia	very large crude carrier	LCA
	Lee et al. [67]	MGO; LNG; hydrogen	ferry	LCA
	Solakivi et al. [11]	MDO; LSMGO; LNG; methanol; biodiesel; e-fuels (hydrogen, ammonia)	ro-ro ship	Economic analysis
	Koričan et al. [68]	Diesel; electricity; methanol; LNG; ammonia; B20; hydrogen	fishing vessel (trawler)	LCA; LCCA
2021	Fan et al. [69]	Diesel; LNG; electricity	container ship; bulk carrier	LCA; LCCA
	Perčić et al. [70]	Diesel; electricity; methanol; LNG; hydrogen; ammonia; B20	inland navigation ships (tanker; small passenger ship; dredger)	LCA; LCCA
	Korberg et al. [36]	Biofuels, bio-e-fuels, and e-fuels (methanol; DME; diesel; liquefied methane gas; LBG; ammonia); hydrotreated vegetable oil; MGO; hydrogen	ro-ro passenger ship; general cargo ship, bulk carrier; container ship	Economic analysis
2020	Perčić et al. [62]	Diesel; electricity; methanol; DME; CNG; LNG; hydrogen; ammonia; B20	ferry	LCA; LCCA
	Spoof-Tuomi and Niemi [63]	MDO; LNG; LBG	ferry	LCA
	Hwang et al. [71]	MGO; LNG; hydrogen	ferry	LCA

### 1.3. Emissions from the Fishing Sector

The fishing sector represents a great part of the food source and the economy of countries with access to the sea. According to the Food and Agriculture Organisation (FAO), more than half of the world's fish production is generated by developing countries. China is the world leader in the number of captured fish, while Norway is the leader in Europe [72]. Fishing vessels come in different sizes, equipped with different types of gear depending on the target species. They operate on unfixed routes and change course frequently, which makes their power needs highly variable. Around 86% of all motorised fishing vessels have a length of less than 12 m, while less than 2% refer to industrial fishing vessels of over 24 m in length and more than 100 GT [73].

Fishing activities affect aquatic ecosystems in terms of visible pollution such as plastic litter and oil spills, invisible pollution such as microplastics and pollutant dumping (different chemicals), underwater noise, bycatch, ghost fishing, over-exploitation of fish, etc. [74]. Fossil fuel consumption is the most significant environmental problem related to fishing activities, affecting the environment and human health [75,76]. Most fishing vessels are powered by conventional fossil marine fuels, like MDO and Marine Gas Oil (MGO), whose combustion results in GHGs, NO<sub>x</sub>, SO<sub>x</sub>, and PM, contributing to global warming and acidification [77]. The fishing sector itself accounts for 1.2% of global oil consumption, which results in the release of 134 million tonnes of CO<sub>2</sub> emissions into the atmosphere [78].

To support sustainable fishing and reduce harmful emissions, replacing traditional power systems with alternative ones fuelled with cleaner fuels needs to be performed. Koričan et al. [68] analysed the environmental and economic impact of several alternative

fuels implemented on a trawler that performs fishing activities in the Adriatic Sea. The LCA comparison of different powering options indicated that the use of ammonia on board results in the highest life-cycle GHG emissions. The most environmentally friendly solution is a fully electrified vessel. From an economic point of view, the LCCA results showed that hydrogen is the most expensive option for the trawler, while the most cost-efficient option is the use of methanol as an alternative fuel. Kim et al. [20] analysed LPG and bio-LPG compared to conventional marine fuels for fishing vessels. The performed LCA indicated that LPG results in 30% lower GHG emissions than diesel-powered fishing vessels, while bio-LPG can reduce GHGs by over 65%. The nexus between all-electric fishing vessels and Isolated Energy Systems (IES) with a high share of renewables was investigated by Koričan et al. [79]. The study confirmed that all-electric ships, charged in island grids, can reduce the critical excess of electricity production, operating costs of IES, and the emissions of CO<sub>2</sub>.

#### 1.4. The Aim of This Paper

This paper reviews alternative marine fuels that can be used for fishing vessels and provides environmental and economic analyses of their application in a purse seiner operating in the Adriatic Sea. Koričan et al. [68] already investigated different alternative fuels in a trawler. However, their study lacks an analysis of various emissions and their impact on acidification, eutrophication, and aerosol formation, which significantly affect human health, the atmosphere, and the marine ecosystem. Also, it does not provide insights into the applicability of alternative fuels for purse seiners due to their significantly different operating profile.

By performing an LCA and LCCA, the life-cycle emissions (GHGs, NO<sub>x</sub>, SO<sub>x</sub>, and PM) and lifetime costs of different alternative fuels (LNG, LBG, LPG, methanol, DME, electricity, hydrogen, ammonia, biodiesel) are investigated. Environmental and economic analyses of a conventional marine fuel, i.e., diesel, onboard a purse seiner serve as a baseline scenario for the final LCA and LCCA comparison of the considered fuels, thus highlighting the most environmentally friendly and economical power system option.

## 2. Methodology

### 2.1. Life-Cycle Assessment

An LCA is a standardised method that offers a holistic approach to assess the environmental impact related to the released emissions and energy used throughout the life-cycle of a product, process, or system [80]. According to ISO guidelines (ISO 14040) [81], an LCA has four fundamental phases: goal and scope, inventory analysis, impact assessment, and interpretation.

The first phase of an LCA represents the definition of its goal, scope, functional unit, system boundary, and the identification of data and impact categories. The Functional Unit (FU) is used to compare the investigated power systems on the same basis, and for this assessment, the FU is the lifetime of a ship, i.e., 20 years. The investigated emissions can be divided into three groups. The first group represents emissions from the Well-to-Tank (WTT) phase, which includes raw material extraction, fuel production, and distribution to the ship. The second group are emissions released during the ship's operation (the Tank-to-Wake (TTW) phase). The third group of emissions belongs to the Manufacturing (M) phase, related to the manufacturing process of the major elements of a power system (engine, fuel cell, battery, etc.).

Emissions from the WTT and M phases were obtained using the LCA software GREET 2022 [82], whose database contains many products (fuels) and stationary and transportation processes related to their life-cycles. The TTW phase refers to the ship's operation, i.e., fishing activities. During that time, fuel is used onboard the ship for its propulsion, gear operation, and other activities (hotelling, refrigeration of fish, etc.). Fuel combustion results



in tailpipe emissions,  $E_{TTW}$  (kg), which are calculated by multiplying emissions factors,  $EF$  (kg gas/kg fuel), by fuel consumption,  $FC$  (kg), according to the following equation:

$$E_{TTW} = EF \cdot FC, \quad (1)$$

where  $EF$ s are obtained from [22,62,83–85] and are presented in Table 3.

**Table 3.** Emission factors,  $EF$  (g/kg) for different fuels [22,62,83–85].

	$EF$ (g/kg)							
	MDO	LNG	LPG	Methanol	DME	LBG	Biodiesel	Ammonia
CO <sub>2</sub>	3206	2750	3015	1375	1927	-	-	-
CH <sub>4</sub>	0.06	51.6	0.006	-	-	51.6	0.06	-
N <sub>2</sub> O	0.15	0.11	0.025	-	-	0.11	0.15	0.0003
NO <sub>x</sub>	61.21	7.83	3.1	8	8	7.83	61.21	0.003
SO <sub>x</sub>	2.64	0.02	0.03	-	-	0.02	2.64	0
PM	1.02	0.18	0.12	-	-	0.18	1.02	0

Total life-cycle emissions,  $E_i$  (kg), are calculated by summing the emissions of a particular gas  $i$  (e.g., CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>O, SO<sub>x</sub>, NO<sub>x</sub>, PM) from each LCA phase, namely the M, WTT, and TTW phase:

$$E_i = E_{WTT,i} + E_{TTW,i} + E_{M,i}. \quad (2)$$

The third phase of an LCA is life-cycle impact analysis, which was carried by means of GREET 2022.

Global Warming Potential,  $GWP$ , (kg CO<sub>2</sub>-eq), was calculated by using CO<sub>2</sub>-equivalent (CO<sub>2</sub>-eq) factors over 100 years (CO<sub>2</sub>: 1; CH<sub>4</sub>: 36; N<sub>2</sub>O: 298), as in the following equation [86]:

$$GWP = 1 \cdot E_{CO_2} + 36 \cdot E_{CH_4} + 298 \cdot E_{N_2O}. \quad (3)$$

The contribution of a particular gas to acidification was evaluated by calculating Acidification Potential,  $AP$  (kg SO<sub>2</sub>-eq), obtained by multiplying the emissions of an acidifying gas by SO<sub>2</sub>-equivalence factors [86]:

$$AP = 1 \cdot E_{SO_x} + 0.7 \cdot E_{NO_x} \quad (4)$$

Aerosol Formation Potential,  $AFP$  (PM<sub>2.5</sub>-eq), was obtained by multiplying emission quantities by PM<sub>2.5</sub> equivalence factors (PM<sub>10</sub>: 0.5; SO<sub>x</sub>: 0.54; NO<sub>x</sub>: 0.88) [86]:

$$AFP = 0.5 \cdot E_{PM_{10}} + 0.54 \cdot E_{SO_x} + 0.88 \cdot E_{NO_x} \quad (5)$$

## 2.2. Life-Cycle Cost Assessment

This economic analysis includes investment, fuel, maintenance costs (costs of maintaining the power system and equipment replacement), and carbon tax for ship power systems that produce tailpipe emissions.

As previously stated, the carbon tax will be implemented in the shipping sector in 2024, and at first, it will be applied to commercial cargo and passenger ships of above 5000 GT, but this work investigates the possibility of its extension to other ship types. The current price of a carbon allowance (September 2023) is around EUR 85/t of CO<sub>2</sub>, but the International Energy Agency predicts that this value will grow up to EUR 238/t of CO<sub>2</sub> by 2050 [87]. According to the World Energy Outlook [88], there are three Carbon Allowance (CA (EUR/t CO<sub>2</sub>)) scenarios for 2030, 2040, and 2050, i.e., the State Policies Scenario (SPS), Announced Pledges Scenario (APS), and Net Zero Emissions by 2050 Scenario (NZES), where:

- SPS: current policies and today's policy intentions and targets for the EU;

- APS: advanced economies with net zero emissions pledges (including all OECD countries except Mexico);
  - NZES: advanced economies with net zero emissions pledges (including all regions).
- These scenarios are presented in Figure 3, where values for other years are obtained by interpolation.

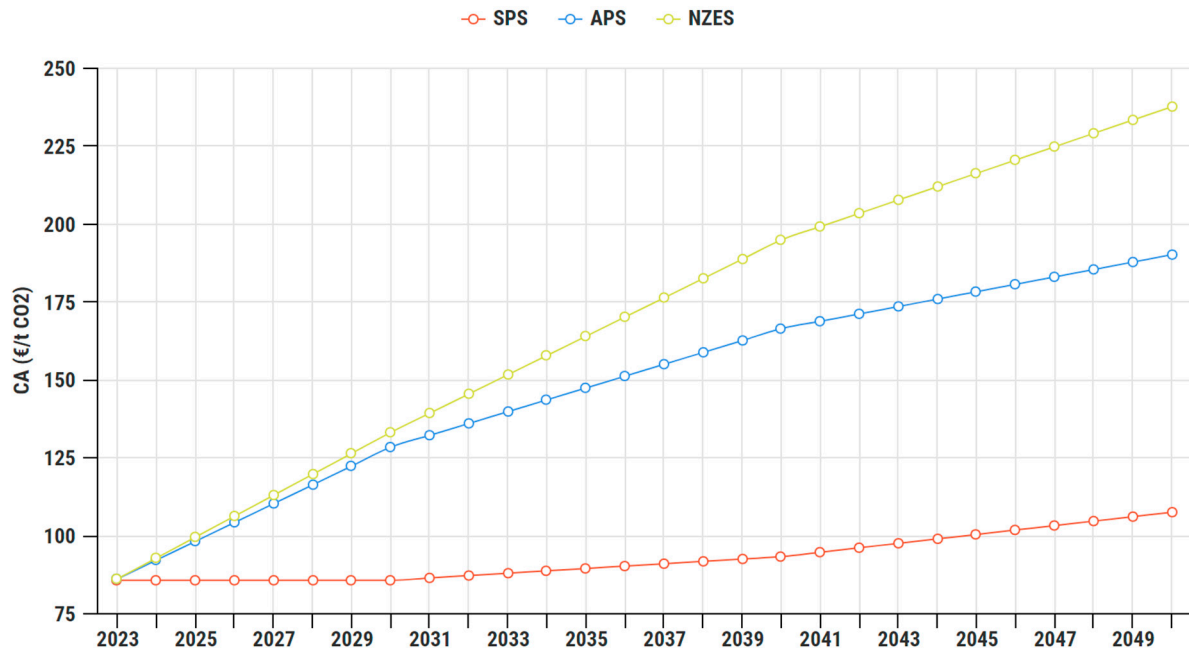


Figure 3. Carbon taxation scenarios.

The cost of CO<sub>2</sub> emissions only applies to ship power systems that result in tailpipe emissions (biofuels are exempted from the tax). Their annual CO<sub>2</sub> emissions from the TTW phase are then multiplied by the CA of a particular year to obtain the carbon tax for that same year.

### 3. Case Study: Purse Seiner in the Adriatic Sea

#### 3.1. Ship Particulars and Operative Profile

The Croatian fishing fleet consists of 7808 fishing vessels, whose fishing activities result in nearly 6% of the total catch in the Mediterranean area. Vessels of less than 6 m in length constitute 56.4% of the fleet, while 36.4% of the fleet are vessels between 5 and 12 m long. However, purse seiners 24 to 40 m in length are responsible for 55% of the landing value and 90% of the landing weight [89,90].

The main particulars of the considered purse seiner are presented in Table 4.

Table 4. Main particulars of considered purse seiner [89].

Length overall, (m)	32.28
Breadth, m	7.40
Draught, m	2.88
GT	182
Main engine power, $P_{ME}$ (kW)	480
Installed auxiliary power, $P_{AE}$ (kW)	370

Fuel consumption during fishing trips highly depends on the operating profile, which for a purse seiner involves several steps, as presented in Figure 4.

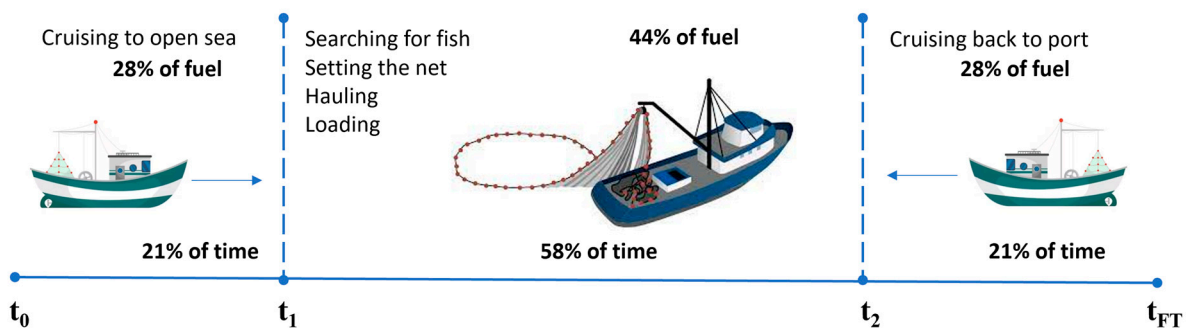


Figure 4. Typical operating profile of a purse seiner.

Data on operating times are crucial for investigating the energy consumption of purse seiners. Their working time varies daily and depends on weather conditions and fish season (and on whether catch limitations are in force) [91]. A typical purse seiner follows the timetable detailed in Figure 4: starting the fish trip at time  $t_0$ , cruising to the open sea till time  $t_1$ ; then, the fishing operation, i.e., harvesting the fish, occurs till time  $t_2$ , when the purse seiner starts to return to the port.

A number of Croatian fishing vessels were equipped with a fuel monitoring system, GPS, and accessory switches by the authors, providing information about their use of particular engines (main and auxiliary engines). The monitoring system was connected to the software “MAPON”, which collects real-time data on the fishing trip (route, time, location, etc.) [92] (Figure 5).

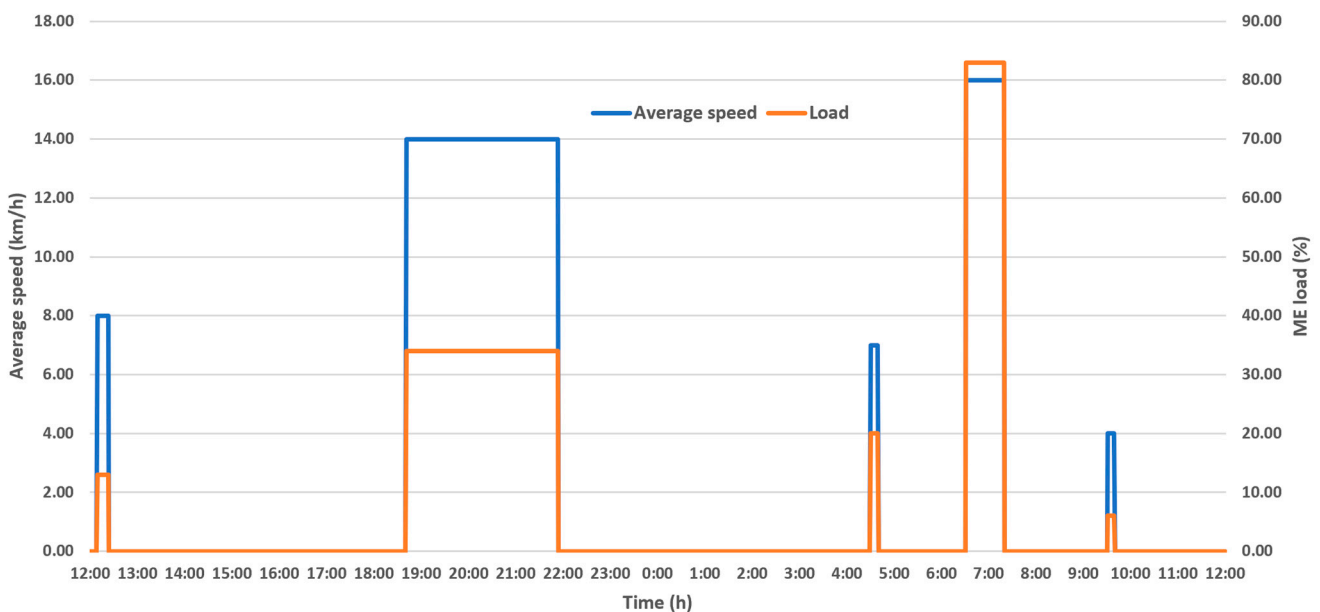


Figure 5. Load profile of a purse seiner on a random fishing trip.

Using data from MAPON, the load profile of a purse seiner on a random fishing trip is presented in Figure 5. It describes how much time the ship spends at which engine speeds and loads, and it relates only to the main engines. Bearing in mind that fishing vessels do not operate on fixed routes and their fishing trips vary, an average ME load of 56% is used within this paper.

Koričan et al. [93] investigated the operating profiles of several Croatian fishing vessels (purse seiners and trawlers) with MAPON and concluded that for purse seiners, the average daily operating time of the main engines ( $t_{ME}$ ) is four hours, while for auxiliary engines ( $t_{AE}$ ), it is 15 h. Due to limitations of work quotas (20 days per month) and the suspension

of fishing due to the restoration of fish stock, they reported the operating time during the year to be around 200 days [89].

The average power of a ship,  $P_{ave}$  (kW), that is required for the ship’s operation (propulsion, fishing, hotelling, gear, etc.) is calculated with the following equation:

$$P_{ave} = P_{ME,ave} + P_{AE,ave} \tag{6}$$

where  $P_{ME,ave}$  (kW) is obtained by multiplying the power of a main engine by 0.56 (average load of 56%), while  $P_{AE,ave}$  (kW) is calculated according to the following equation [93]:

$$P_{AE,ave} = 0.388 \cdot P_{ME,ave} \tag{7}$$

Furthermore, the energy consumption of a ship,  $EC_A$  (kWh), is calculated on an annual basis as follows:

$$EC_A = P_{ME,ave} \cdot t_{ME,A} + P_{AE,ave} \cdot t_{AE,A} \tag{8}$$

where  $t_{ME,A}$  (h) and  $t_{AE,A}$  (h) refer to the annual operating time of the main engine and auxiliary engines, which equal 800 h and 3000 h, respectively. The energy needs and ECA for each considered alternative power system are equal to those for the existing diesel-powered ship.

Currently, fishing vessels in Croatia are completely powered by diesel fuel. The annual fuel consumption of diesel,  $FC_{D,A}$  (kg), is calculated with the equation:

$$FC_{D,A} = EC_A \cdot SFC_D \tag{9}$$

where  $SFC_D$  (kg/kWh) refers to the specific fuel consumption of diesel of 0.190 kg/kWh, which is calculated for the average load of 56% by following the guidelines within the IMO’s fourth GHG study [94].

### 3.2. LCA Models for Different Power Systems

#### 3.2.1. The LCA of a Diesel-Powered Ship

Before analysing the considered alternative power systems, the LCA of the power system currently used in the fishing sector (diesel-powered ship) needs to be performed. It serves as a baseline scenario in the final comparison of the environmental impact of possible fishing fuels. The energy needs of the diesel-powered ship are presented in Section 3.1.

The processes included in the LCA of a diesel-powered ship are shown in Figure 6.

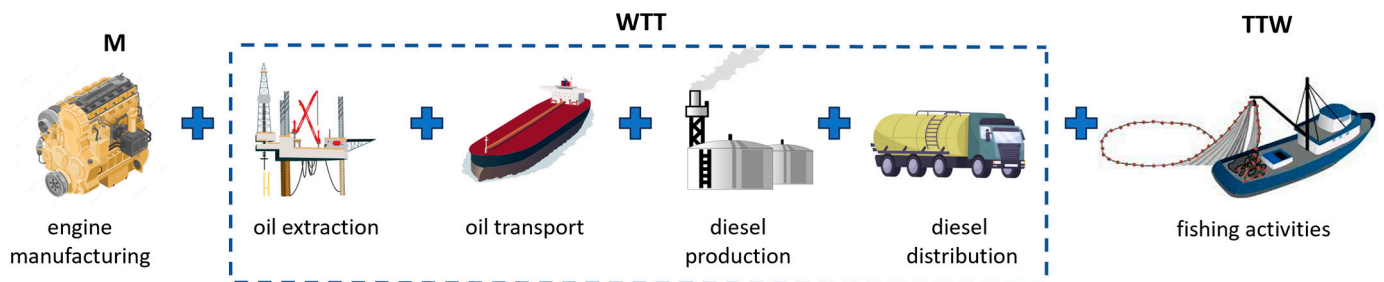


Figure 6. Processes included in the LCA of a diesel-powered ship.

The environmental impact of diesel engines is included within the M phase, which refers to the manufacturing process of the materials that the engine consists of. As presented by Perčić et al. [62], the weight of each material that serves as an input to GREET 2022 is calculated by multiplying the materials’ weight ratios by the weight of the engine  $m$  (t), calculated by the following equation [62]:

$$m = \frac{2 \cdot P_{ave}}{450} \tag{10}$$

The WTT phase of diesel includes crude oil extraction in the Middle East and its transportation to Croatia via tanker for 4000 km. Once the oil is imported at the Croatian terminal, it is brought to the refinery in Rijeka through the oil pipeline. At the refinery, the oil is refined. The produced diesel is then distributed to the pump in the port by tank truck for 100 km.

The TTW phase refers to the combustion of diesel in the marine engine. Depending on their emission factor (Table 3), these emissions are calculated with Equation (1).

### 3.2.2. The LCA of an LNG-Powered Ship

The uptake of LNG as an alternative fuel onboard fishing vessels is increasing [37]. LNG-powered ships are powered by dual-fuel engines in which LNG and diesel are used, e.g., modern dual-fuel by Wärtsilä [16]. It is assumed that the purse seiner considered operates only in a dual-fuel mode with 95% LNG ( $x_{LNG}$ ) and 5% diesel ( $x_{P-LNG}$ ), used as a pilot fuel to initiate combustion. According to Perčić et al. [62], general equations for the calculation of fuel consumption for a dual-fuel engine are:

$$FC_f = x_f \cdot EC \cdot SFC_f, \tag{11}$$

$$FC_{p-f} = x_{p-f} \cdot EC \cdot SFC_{p-f}, \tag{12}$$

where  $x$  represents the share of fuel in a dual-fuel engine, while the subscripts  $f$  and  $p-f$  refer to the second and pilot fuels, respectively. Specific fuel consumptions are obtained from [62]. The processes included in the LCA of an LNG-powered ship are presented in Figure 7.

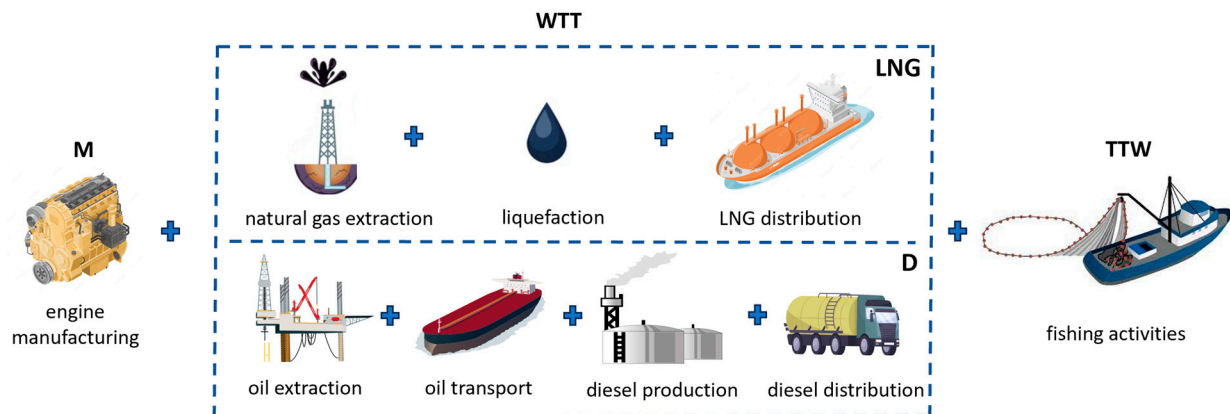


Figure 7. Processes included in the LCA of an LNG-powered ship.

The environmental impact of the engine is the same as that of the diesel engine in Section 3.2.1. The WTT phase includes natural gas extraction in Qatar, where, before transportation to Croatia (for 7000 km), the natural gas is liquefied on site. According to Perčić et al. [62], the general equation for the calculation of TTW emissions released from dual-fuel engines is:

$$E_{TTW,i} = EF_{f,i} \cdot FC_f + EF_{D,i} \cdot FC_{p-f}, \tag{13}$$

where  $EF_f$  and  $EF_D$  refer to the emission factors of the second fuel and pilot fuel (diesel). The emission factors are presented in Table 3. The methane slip in the TTW phase is calculated by multiplying 5.5 g CH<sub>4</sub>/kWh [95] by energy consumption and added to CH<sub>4</sub> emissions calculated with Equation (13).

### 3.2.3. The LCA of an LPG-Powered Ship

In this paper, LPG is used onboard a purse seiner in a dual-fuel engine suitable for LPG. It is assumed that ships operate only in a dual-fuel mode with 95% LPG ( $x_{LPG}$ ) as the second fuel and 5% diesel ( $x_{P-LPG}$ ) as the pilot fuel. The fuel consumption of an LPG-powered ship

is calculated by Equations (11) and (12). Specific fuel consumptions are obtained from [96]. The processes included in the LCA of an LPG-powered ship are presented in Figure 8.

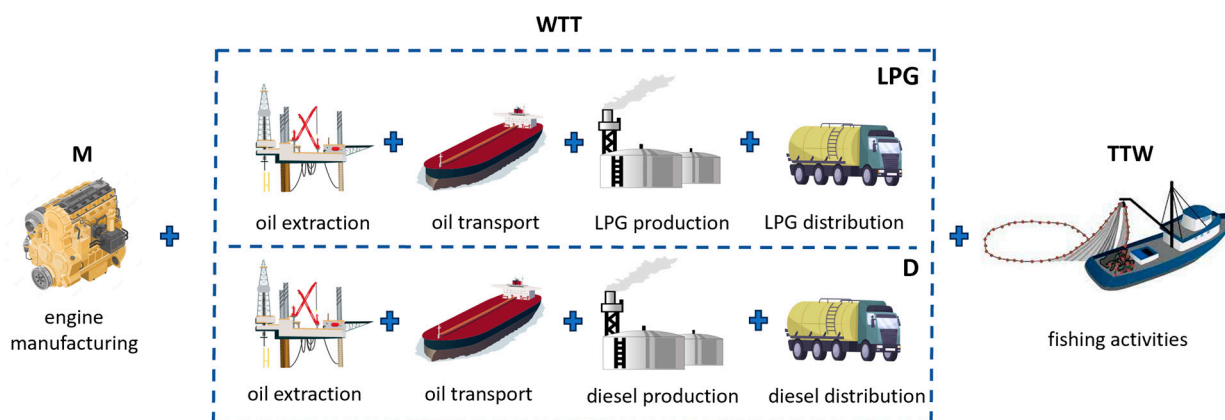


Figure 8. Processes included in the LCA of an LPG-powered ship.

The environmental impact of the engine is the same as that of the diesel engine in Section 3.2.1, while TTW emissions are calculated based on Equation (13), with emission factors for LPG and diesel presented in Table 3. The WTT phase processes of LPG and diesel as pilot fuels are the same (Section 3.2.1), except the process of fuel production in the Croatian refinery. LPG is assumed to be produced in Europe and then transported to Croatia via tank truck for 2000 km.

### 3.2.4. The LCA of a Methanol-Powered Ship

Onboard ships, methanol is mainly used as a second fuel in dual-fuel engines. For this assessment, it is assumed that the purse seiner operates only in a dual-fuel mode with 95% methanol and 5% pilot fuel (diesel). Specific fuel consumption is obtained from [97], while the fuel consumption of a methanol-powered ship is calculated with Equations (11) and (12). The processes included in the LCA of a methanol-powered ship are presented in Figure 9.

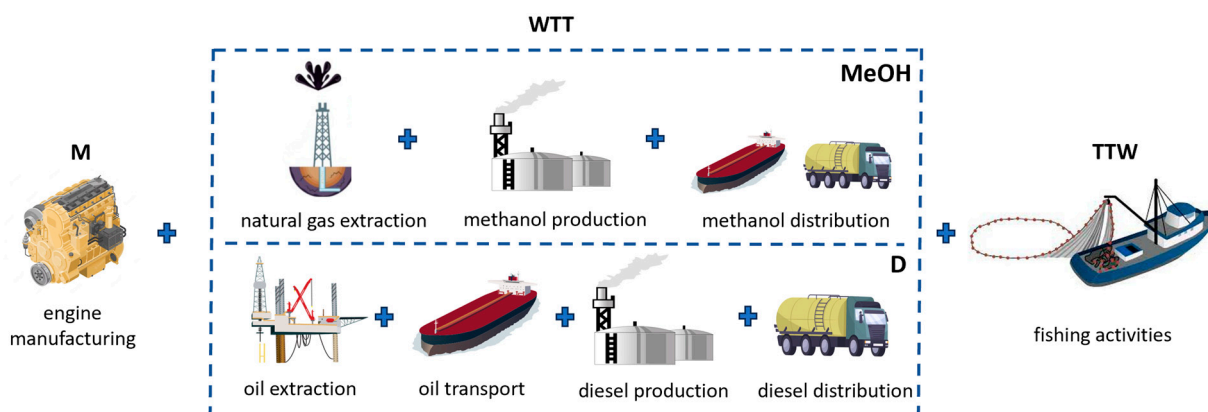


Figure 9. Processes included in the LCA of a methanol-powered ship.

The environmental impact of the engine is the same as that of the diesel engine in Section 3.2.1, while TTW emissions are calculated based on Equation (13), with emission factors for methanol and diesel presented in Table 3.

### 3.2.5. The LCA of a DME-Powered Ship

In contrast to the other low-carbon fuels considered, DME is a compression ignition fuel, and in this paper, it is assumed to be used in a modified ICE. Fuel consumption is

calculated with Equation (9) [65]. The processes included in the LCA of a DME-powered ships are presented in Figure 10.

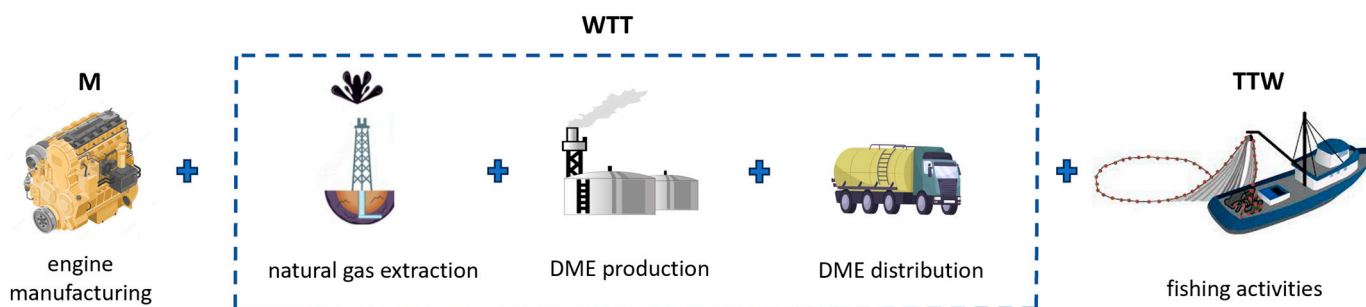


Figure 10. Processes included in the LCA of a DME-powered ship.

The environmental impact of the engine is the same as that of the diesel engine in Section 3.2.1, while TTW emissions are calculated based on Equation (1), with emission factors for DME presented in Table 3. The WTT phase of DME includes natural gas extraction, the production of DME, and its distribution to the port via tank truck for 1500 km.

### 3.2.6. The LCA of a Biodiesel-Powered Ship

Biodiesel is compatible with the existing distribution infrastructure and with diesel engines. Although its use is limited to a blend with diesel, with minor modifications, pure biodiesel can be used [34]. In this paper, pure biodiesel, i.e., B100 (100% biodiesel), and biodiesel–diesel blend B20 (20% biodiesel; 80% diesel) are investigated. It is assumed that the fuel consumption of a diesel-powered ship is the same as the fuel consumption of a biodiesel-powered ship. The processes included in the LCA of a B20-powered ship and the LCA of a B100-powered ship are presented in Figures 11 and 12, respectively.

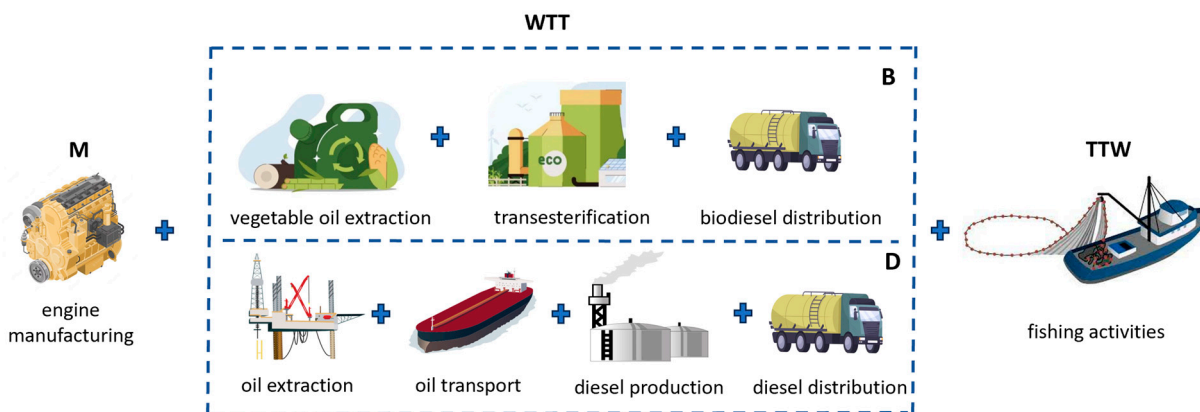


Figure 11. Processes included in the LCA of a B20-powered ship.

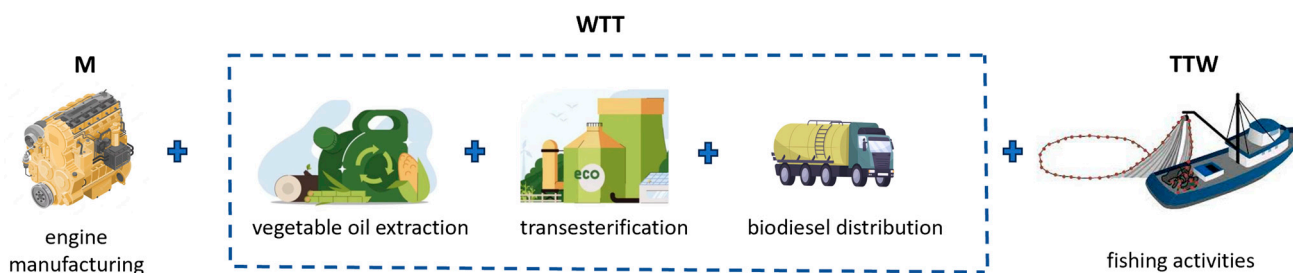


Figure 12. Processes included in the LCA of a B100-powered ship.

The environmental impact of the engine is the same as that of the diesel engine in Section 3.2.1, while TTW emissions are calculated based on Equation (1), with emission factors for biodiesel and diesel presented in Table 3. The WTT phase of biodiesel includes soy oil extraction from soybeans, the process of transesterification by which biodiesel is produced, and the transportation of biodiesel to the refuelling station in the port via tank truck for 1000 km.

### 3.2.7. The LCA of an LBG-Powered Ship

LBG, known as bio-LNG or renewable LNG, can be produced from various sources. LBG production from animal waste is considered in this study.

Since LBG and LNG are interchangeable, LBG is used like LNG, in a dual-fuel engine with diesel as the pilot fuel. Specific fuel consumption and equations for the calculation of fuel consumption are presented in Section 3.2.2. The processes included in the LCA of an LBG-powered ship are presented Figure 13.

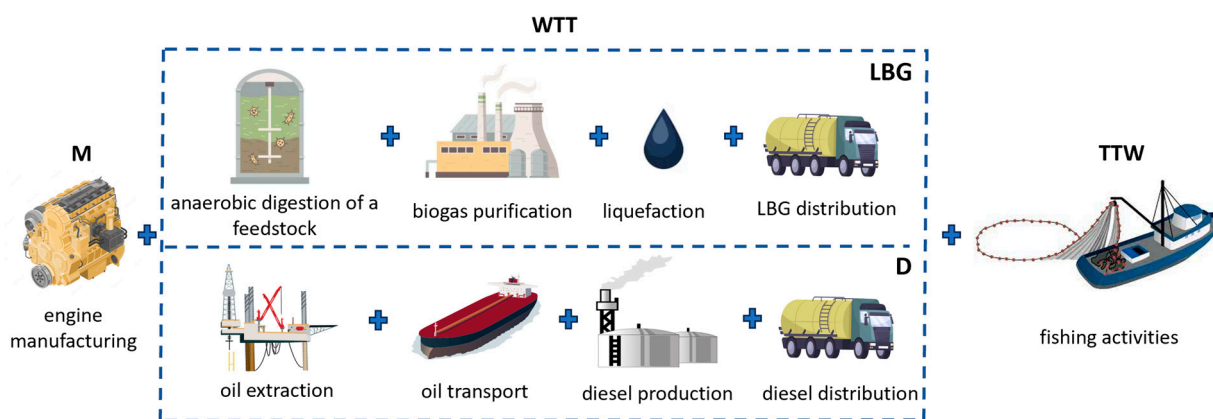


Figure 13. Processes included in the LCA of an LBG-powered ship.

The environmental impact of the engine is the same as that of the diesel engine in Section 3.2.1, while TTW emissions are calculated based on Equation (13), with emission factors for LBG and diesel presented in Table 3. The methane slip in the TTW phase is considered in the same manner as for LNG. The WTT phase of LBG includes the anaerobic digestion of a feedstock (animal waste), the process of biogas upgrading (biogas purification process, during which methane is separated from CO<sub>2</sub> and other gases to form biogas), liquefaction of biogas, and its transportation to storage in the port via tank truck for 2000 km.

### 3.2.8. The LCA of a Hydrogen-Powered Ship

In this paper, grey hydrogen (produced by natural gas) and green hydrogen (produced from Renewable Energy Sources (RESs)) are investigated to gain an insight into their feasibility, environmental friendliness, and economic performance as marine fuels.

Hydrogen represents an ideal fuel for fuel cells. In this paper, a high-temperature Solid Oxide Fuel Cell (SOFC) is selected for further assessment. The annual fuel consumption of hydrogen in a SOFC, i.e.,  $FC_{SOFC-H}$  (kg), is calculated with the following equation [86]:

$$FC_{SOFC-H} = \frac{EC_{SOFC}}{\eta_{SOFC} \cdot LHV_H}, \tag{14}$$

where  $\eta_{SOFC}$  refers to SOFC efficiency (60%),  $LHV_H$  represents lower heating value of hydrogen (kWh/kg), Table 1, while  $EC_{SOFC}$  (kWh) refers to the annual energy consumption of an SOFC-powered ship.

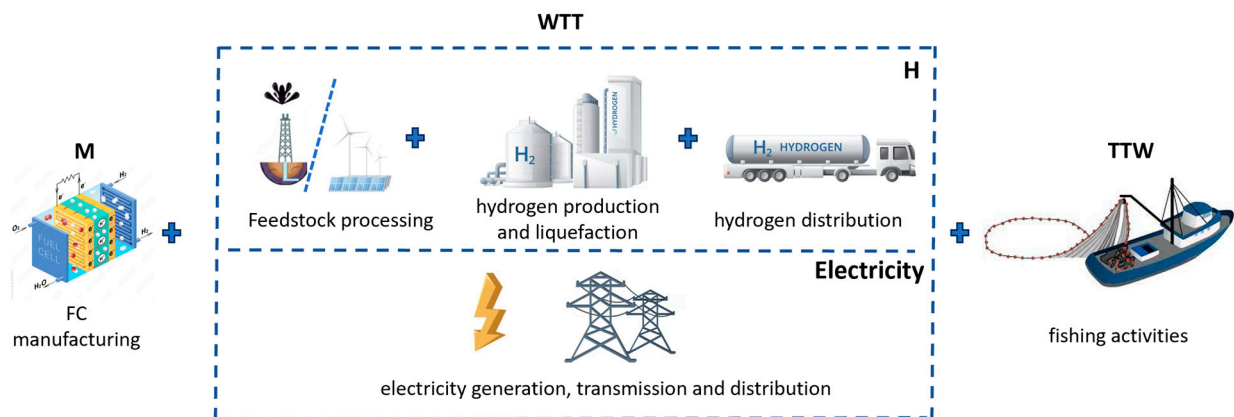
Selected SOFCs provide fuel flexibility and higher energy efficiency than low-temperature fuel cells, such as a Proton Exchange Membrane Fuel Cell (PEMFC), but they require higher temperatures for operation. The time required for the fuel cell system to reach its operating



temperature is referred to as the start-up time, which for the SOFC equals 30 min [98]. The energy required for heating the fuel cell system,  $EH_{FC}$  (kWh), is calculated with the following equation [86]:

$$EH_{FC} = 0.015 \cdot 6.7 \cdot P_{SOFC}. \quad (15)$$

The processes included in the LCA of a hydrogen-powered ship are presented in Figure 14. During the ship's operation, there are no tailpipe emissions, i.e., TTW emissions are equal to zero.



**Figure 14.** Processes included in the LCA of a hydrogen-powered ship (FC-H).

The M phase refers to the process of SOFC manufacturing. Its environmental impact is analysed through the weights of the materials used for SOFC manufacturing [26] as inputs for GREET 2022. Its replacement is considered after 20,000 working hours [86]. The WTT phase of hydrogen includes the processes of feedstock processing, hydrogen production and liquefaction, and finally, distribution to the port. Feedstock processing depends on hydrogen origin. Grey hydrogen feedstock processing refers to natural gas extraction, while the feedstock processing of green hydrogen refers to the production of electricity by RESs. It is assumed that each type of hydrogen is produced in Western Europe, liquefied, and transported to Croatia via tank trucks for 1000 km. Besides the WTT phase of hydrogen, the LCA also contains the WTT phase of electricity, since onshore electricity is used for the start-up of the fuel cells, and it includes electricity generation, transmission, and distribution. The sources included in the European electricity mix in the GREET 2022 software are used for electricity generation in Croatia.

### 3.2.9. The LCA of an Ammonia-Powered Ship

Ammonia has been widely investigated as a hydrogen carrier. In this paper, its use onboard in a fuel cell and ICE is analysed. As for the fuel cell, the SOFC is considered because it is fuel-flexible and allows for the fast decomposition of ammonia on hydrogen and nitrogen (due to high operating temperatures). If the PEMFC is used instead of the SOFC, the ammonia would need to go through a cracker and a purifier to ensure the provision of pure hydrogen to the fuel cell. That option results in higher costs and fuel consumption [86].

The electricity consumption, average power, and energy consumption of a ship powered by a SOFC correspond to those of the hydrogen-powered ship described in Section 3.2.8. Ammonia consumption is calculated with the following equation:

$$FC_{SOFC-A} = \frac{EC_{SOFC}}{\eta_{SOFC-A} \cdot LHV_A}, \quad (16)$$

where  $\eta_{SOFC-A}$  refers to the system efficiency of SOFC fuelled with ammonia (55%) [99] and  $LHV_A$  represents lower heating value ammonia (kWh/kg) (Table 1) [89].

The processes included in the LCA of an ammonia-powered ship with the fuel cell (A-H) are presented in Figure 15. During fishing activities, there are no tailpipe emissions, i.e., TTW emissions are equal to zero.

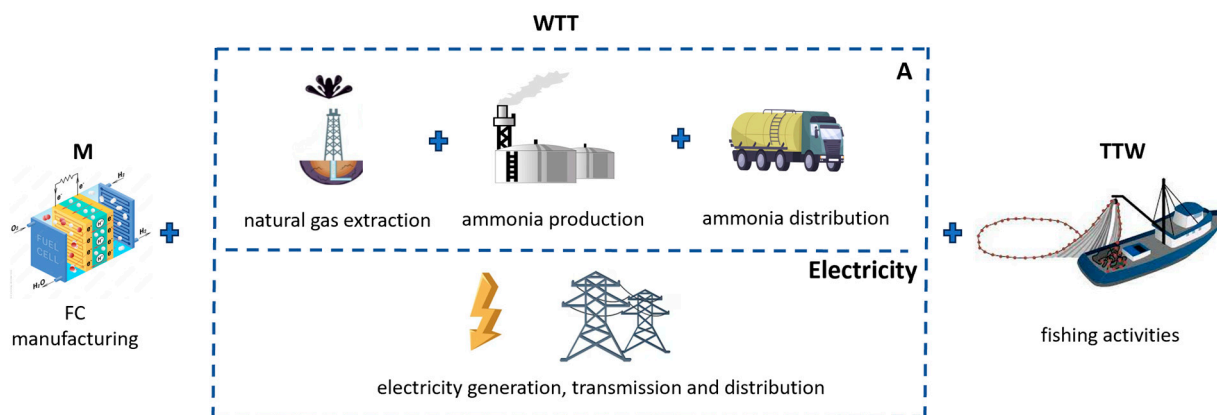


Figure 15. Processes included in the LCA of an ammonia-powered ship (FC-A).

The manufacturing of the SOFC and the WTT phase of electricity correspond to the ones from Section 3.2.8. The WTT phase of ammonia includes natural gas extraction, production of ammonia, and its distribution via tank trucks for 1000 km.

Currently, there are no commercially available ammonia ICEs, but MAN promises their availability in 2024 [100]. A dual-fuel marine engine powered by ammonia and diesel has been investigated in many studies. A pilot fuel (MDO or MGO) is used to initiate combustion in a share of 5–10% [101]. In this paper, the pilot use of 5% is assumed, while specific fuel consumptions are obtained from a study by Huang et al. [66], and they equal 358.6 g/kWh for ammonia and 190 g/kWh for the pilot fuel, respectively. Fuel consumptions can be calculated with Equations (11) and (12).

The processes included in the LCA of an ammonia-powered ship (ICE-A) are presented in Figure 16.

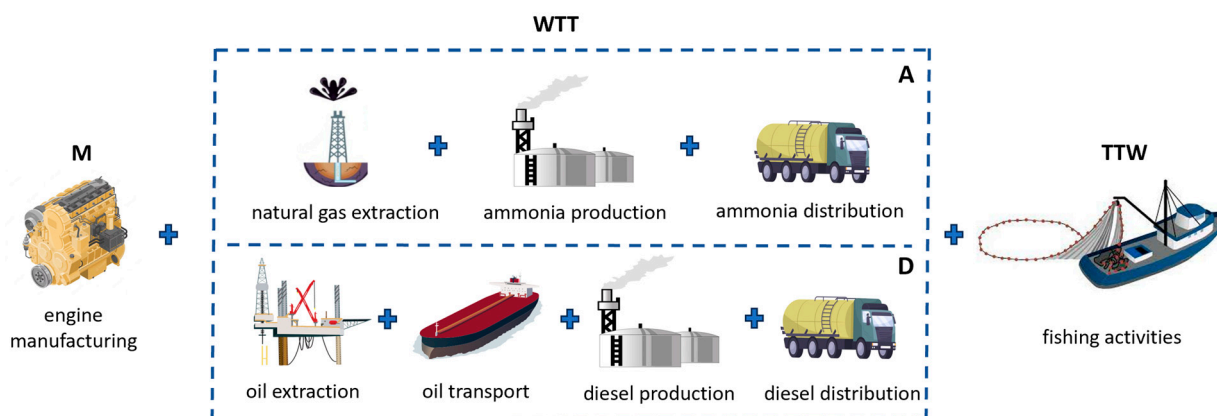


Figure 16. Processes included in the LCA of an ammonia-powered ship (ICE-A).

The environmental impact of the engine is the same as that of the diesel engine in Section 3.2.1, while TTW emissions are calculated based on Equation (13), with emission factors for diesel presented in Table 3. The WTT phase of ammonia corresponds to the WTT phase of ammonia used in a fuel cell.

### 3.2.10. The LCA of an All-Electric Ship

All-electric ships operate solely on battery. There are different types of batteries, but currently, the Li-ion battery stands out with the best performance, low emissions, and high energy density compared to other types [47]. Although fully electrified ships are attractive

alternatives due to zero emissions during their operation, their application highly depends on battery capacity and trip range [44].

It is assumed that battery capacity needs to be sufficient to power the ship for the whole fishing trip. Therefore, battery capacity  $BC$  (kWh) corresponds to daily energy consumption, and it is calculated by the following equation:

$$BC = 1.5 \cdot (P_{ME,ave} \cdot t_{ME} + P_{AE,ave} \cdot t_{AE}). \tag{17}$$

Battery capacity is increased by 50% due to safety, battery degradation, and maintaining state of charge.

The processes included in the LCA of an all-electric ship are battery manufacturing and the WTT phase of electricity (Figure 17), while TTW emissions are equal to zero.

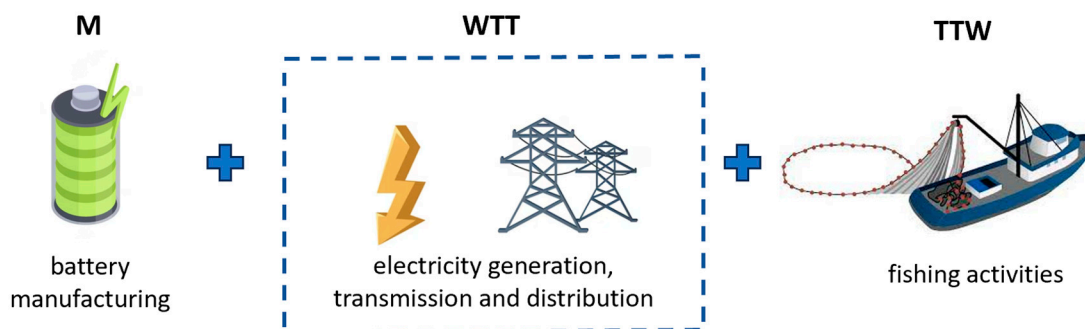


Figure 17. Processes included in the LCA of an all-electric ship.

The M phase refers to the manufacturing of the Li-ion battery. By dividing the required  $BC$  and battery energy density, which for Li-ion battery with nickel manganese cobalt oxide chemistry is 0.22 kWh/kg [102], battery weight is calculated. The battery needs to be replaced after 9000 cycles of charging and discharging. The WTT phase of electricity refers to its generation, transmission, and distribution. The emissions released during electricity production depend on the electricity mix, i.e., sources of energy used. In this paper, the European electricity mix from the GREET 2022 database is used.

### 3.3. LCCA Models for Different Power Systems

The main cost of a ship’s power system is fuel cost. Due to fuel price fluctuations, the minimum and maximum prices in the literature are investigated and then used to calculate the average price of a particular fuel (Table 5). Lifetime fuel costs are then calculated by multiplying annual fuel consumption by the fuel price in a particular scenario,  $LHV$ , or energy consumption (for electricity) and the lifetime of a ship, i.e., 20 years.

Table 5. Fuel prices.

	Fuel Price (EUR/GJ)
Diesel	22.8 [103]
LNG	17.5 [18,63]
LPG	18.6 [42,104]
Methanol	15.3 [105]
DME	10.7 [105]
Biodiesel	34.4 [103]
LBG	25.9 [106]
Hydrogen (grey)	25.8 [42,86]

**Table 5.** *Cont.*

	Fuel Price (EUR/GJ)
Hydrogen (green)	30.2 [42]
Ammonia	20.8 [42,86]
Electricity	10.3 [42]

### 3.3.1. The LCCA of a Diesel-Powered Ship

Investment cost refers to the purchase of a new engine, which is assumed to be EUR 180/kW, while annual maintenance costs are EUR 0.014/kWh [107]. Fuel cost is calculated by multiplying fuel consumption by the fuel price in Table 5, while the carbon tax is calculated as described in Section 2.2.

### 3.3.2. The LCCA of an LNG-Powered Ship

The investment cost of an LNG-powered ship is EUR 1290/kW, and it refers to the retrofitting of an existing ship with a dual-fuel engine for LNG and pilot fuel (diesel), all additional equipment, and an LNG storage tank [42]. The maintenance cost of the considered power system is equal to EUR 0.015/kWh [107]. Fuel cost is calculated by multiplying fuel consumption by fuel prices from Table 5, while the carbon tax is calculated as described in Section 2.2.

### 3.3.3. The LCCA of an LPG-Powered Ship

Retrofitting an existing ship with an LPG power system costs around EUR 750/kW and includes a new engine, storage tanks, and other additional equipment [108]. The maintenance cost of an LPG-powered ship is assumed to be the same as for LNG-powered ship. Fuel cost is calculated by multiplying fuel consumptions by fuel prices from Table 5, while the carbon tax is calculated as described in Section 2.2.

### 3.3.4. The LCCA of a Methanol-Powered Ship

The investment cost for the conversion of a diesel power system to a methanol-powered system is EUR 750/kW, which includes the purchase of a dual-fuel engine and the required equipment [109]. The maintenance cost of a methanol-powered ship is assumed to be the same as that of a diesel-powered ship. Fuel cost is calculated by multiplying fuel consumptions by fuel prices from Table 5, while the carbon tax is calculated as described in Section 2.2.

### 3.3.5. The LCCA of a DME-Powered Ship

Since DME is dehydrated methanol, its fuel price in EUR/kg is the same as that of methanol, while investment and maintenance costs of a methanol-powered ship are increased by 10% due to differences in storage. Fuel cost is calculated by multiplying fuel consumptions by the fuel price from Table 5, while the carbon tax is calculated as described in Section 2.2.

### 3.3.6. The LCCA of a Biodiesel-Powered Ship

The investment and maintenance costs of a biodiesel-powered ship correspond to the ones of a diesel-powered ship. Fuel cost is calculated by multiplying fuel consumption by fuel prices from Table 5.

### 3.3.7. The LCCA of an LBG-Powered Ship

LBG and LNG are interchangeable fuels. Therefore, LBG use as an alternative marine fuel results in investment and maintenance costs equal to the ones of an LNG-powered ship. Fuel cost is calculated by multiplying fuel consumption by fuel prices from Table 5.

### 3.3.8. The LCCA of a Hydrogen-Powered Ship

The investment costs of a fuel cell system fuelled with hydrogen correspond to the price of a SOFC (EUR 2200/kW). However, this cost is increased by 20% due to additional equipment. Lifetime maintenance refers to 10% of investment costs. During the ship's lifetime, the fuel cell is replaced twice, while its price declines by 25% [86]. Fuel cost is calculated by multiplying fuel consumption (hydrogen as fuel for the fuel cell and electricity required for heating the fuel cell system) by fuel prices from Table 5.

### 3.3.9. The LCCA of an Ammonia-Powered Ship

The investment, maintenance, and equipment replacement costs of an ammonia-powered ship with a fuel cell correspond to the costs of a hydrogen-powered ship with a fuel cell as detailed in Section 3.3.8. Fuel cost is calculated by multiplying fuel consumption (ammonia as fuel for the fuel cell and electricity required for heating the fuel cell system) by fuel prices from Table 5.

Besides in a fuel cell, ammonia is investigated as a fuel for ICEs, used in a dual-fuel engine with diesel as the pilot fuel. Investment costs related to the purchase of a new ammonia engine with additional gear and tanks are calculated by multiplying average ship power by a conversion factor of EUR 1330/kW [108]. Annual maintenance cost is equal to 1.5% of the investment cost [101]. Fuel cost is calculated by multiplying fuel consumption by fuel prices from Table 5, while the carbon tax is calculated as described in Section 2.2.

### 3.3.10. The LCCA of an All-Electric Ship

The battery represents the main element of a fully electrified ship. Its cost is calculated by multiplying the required battery capacity by a battery price of EUR 250/kWh [36]. The investment cost of an all-electric ship constitutes 45% of the battery cost, while the remaining 55% is spent on additional equipment [70]. The battery is replaced once in a ship's lifetime, and its price declines by 25%. Maintenance represents 5% of the investment cost, while electricity cost is calculated by multiplying energy consumption by electricity prices from Table 5.

## 3.4. Limitations and Assumptions

The limitations and approximations of this paper are as follows:

- The system boundary of the assessments is placed on the ship, where only the power system is investigated. The other units of a ship (e.g., hull, additional equipment, crew, port operations, etc.) are not considered. However, this approach sufficiently identifies alternative power systems to reduce emissions at a reasonable cost, compared to the configuration of a conventional diesel power system.
- Since the considered purse seiner does not operate on a fixed route and its operative profile varies, an average load of 56% is taken for the calculation of energy needs.
- One of the assumptions in this paper is the simplification of fuel transportation processes. However, stationary processes are a major contributor to emissions from the WTT phase, so this assumption does not have a major impact on total emissions from the WTT phase.
- Storage tank dimensions for a particular fuel (LNG, LBG, hydrogen, etc.) are not considered, which is a limitation for their use onboard small fishing vessels. Such fuel tanks occupy additional space on ships that can be used for different purposes (e.g., for similar energy content, an LNG tank occupies 3–4 times greater a space than an MGO tank) [110]. Nevertheless, environmental and economic analyses performed within the study successfully identified the most appropriate power system configuration that satisfies both criteria.
- Biofuels are assumed to be climate-neutral, and their combustion does not result in CO<sub>2</sub> emissions.
- The environmental impact of dual-fuel engines is assumed to be the same as for diesel engines. Since manufacturing emissions from engine manufacturing are rather small

compared to batteries and fuel cells and their share in overall life-cycle emissions is small, this approach does not result in a great change in the final results.

- When the ship is powered by a dual-fuel engine, it is assumed that it is always operating in dual-fuel mode, and the pilot fuel share is 5% for each power system configuration that includes a dual-fuel engine.
- Despite recent fuel price fluctuations, fuel costs within the LCCA are calculated with average fuel prices obtained from the literature. Sensitivity analysis regarding an increase in fuel price is not considered.
- Another limitation regarding the LCCA is that the costs are investigated without analysing the net present value. However, the LCCA still identifies the most cost-efficient option.
- The use of ammonia in ICEs is still in the development phase, and commercial engines should be available in 2024. It can be assumed that the implementation phase of such a power system would yield different emissions and overall costs than what is obtained in this study. The LCA and LCCA of this power system configuration should be repeated when their technology readiness is higher.

#### 4. Results and Discussion

In the below results, D denotes diesel, MeOH is methanol, AES denotes all-electric ship, A-FC and A-ICE refer to the use of ammonia in the fuel cell and ICE, and H-FC denotes the use of hydrogen in the fuel cell, where hydrogen can be grey or green. Other fuel abbreviations are already explained with the first mention in the paper (LNG, LPG, DME, LBG, B100, B20).

The LCA investigated life-cycle emissions related to ship power systems. The impact categories of climate change, human toxicity, and acidification were selected for analysis, and the results are presented in Figures 18–20.

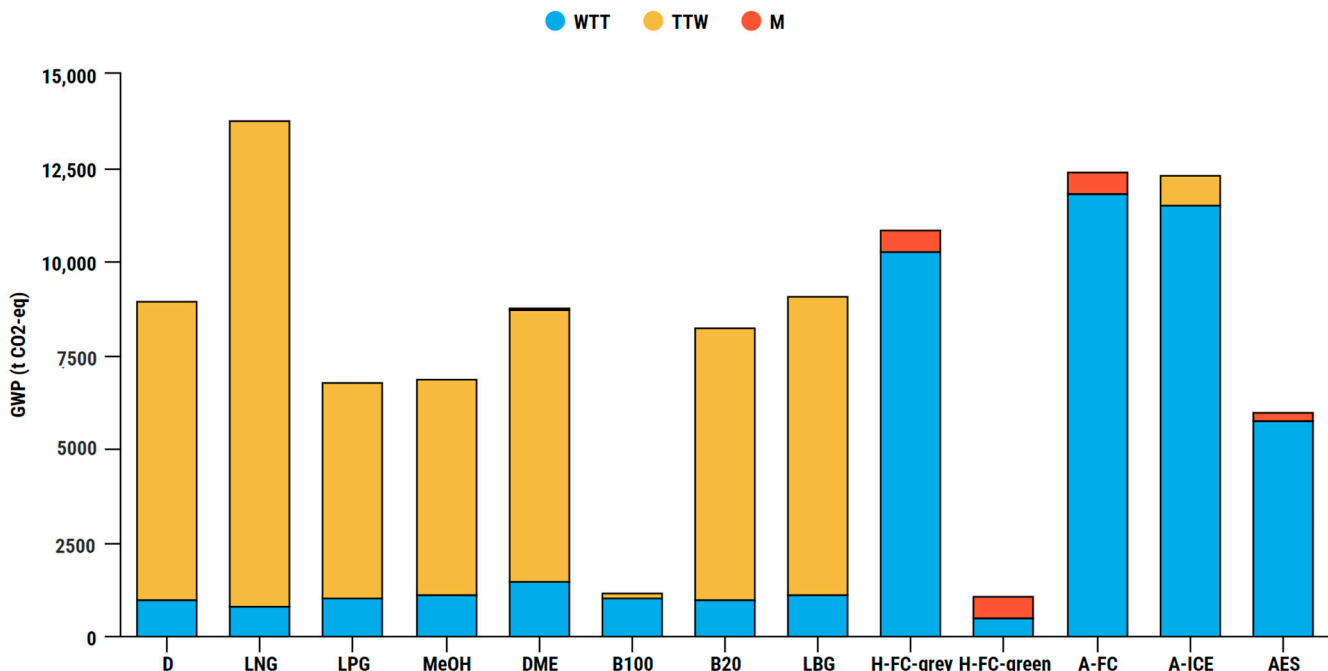


Figure 18. LCA comparison of different power systems (impact category: climate change).

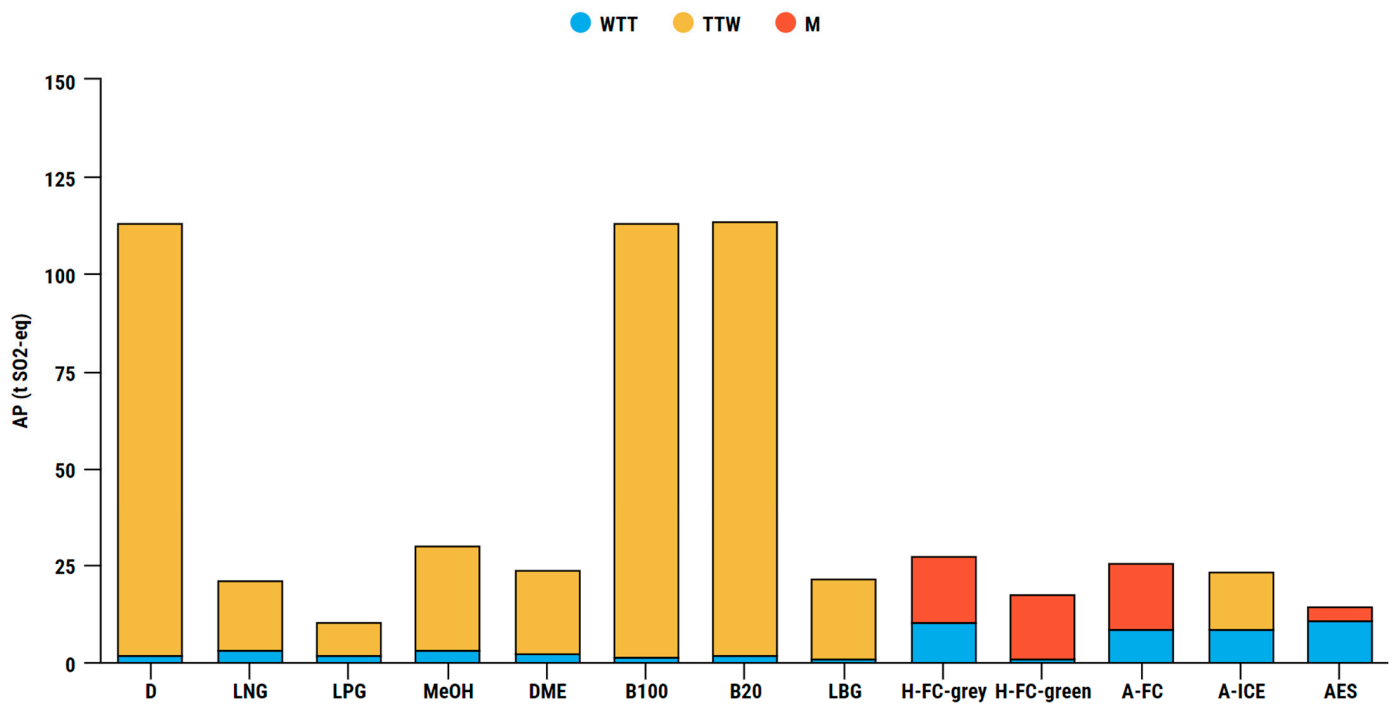


Figure 19. LCA comparison of different power systems (impact category: acidification).

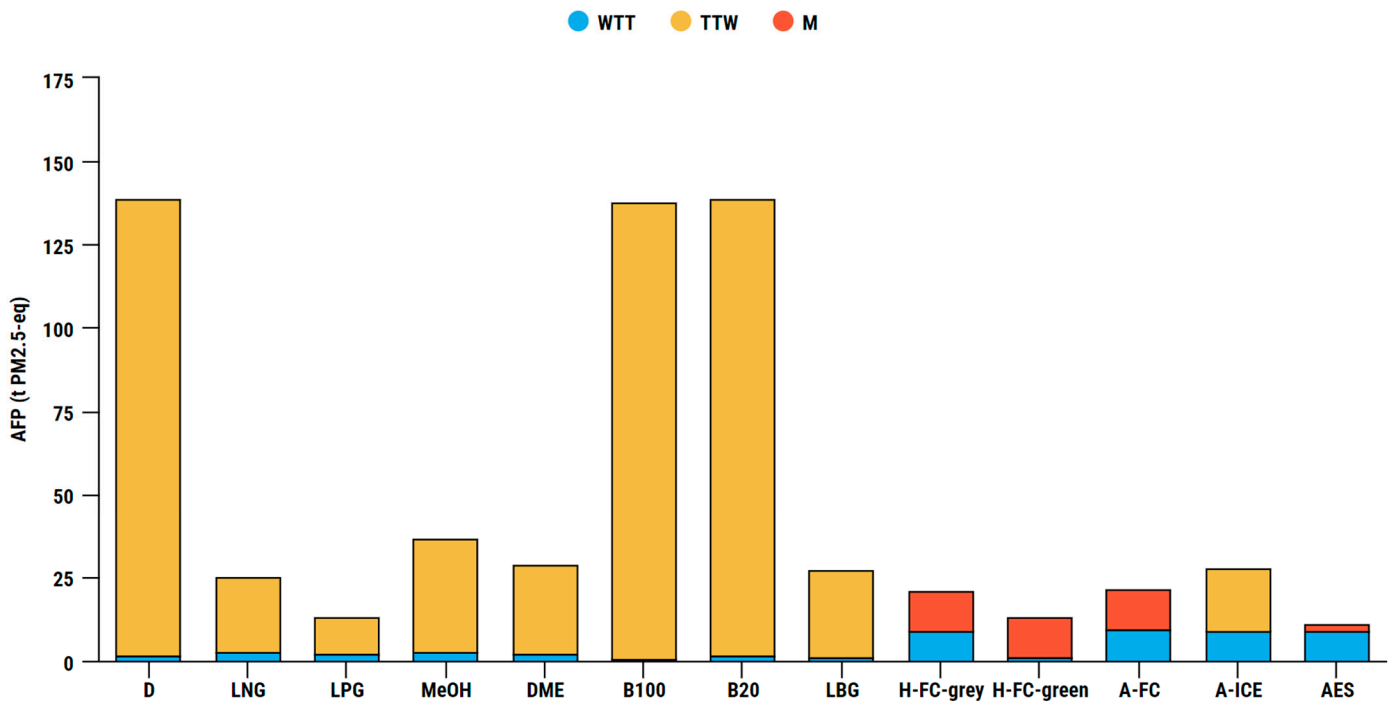


Figure 20. LCA comparison of different power systems (impact category: human toxicity).

According to Figure 18, fossil fuels (diesel and low-carbon fuels) greatly contribute to climate change with a high amount of released GHGs. A major part of these emissions are emissions from TTW (a result of fuel combustion in marine engines). The LCA highlighted green hydrogen, B100, methanol, and electricity as potential alternative fuels whose use instead of diesel would reduce the carbon footprint of the investigated ship. The alternatives that resulted in the highest GHGs are LNG, ammonia (used in fuel cells and ICE) and grey hydrogen (used in a fuel cell).

Regarding acidification (Figure 19), the diesel-powered ship is a major contributor due to the high sulphur content compared to investigated alternatives. Biodiesel–diesel blend (B20) and B100 have similar *AP* values as the diesel-powered ship, while green hydrogen and LPG have the lowest impact. Similar results are presented in Figure 20, where life-cycle emissions are used to calculate the impact on human toxicity. Diesel, B100, and B20 are the greatest contributors, while green hydrogen and LPG result in the lowest emissions.

To gain an insight into their cost-effectiveness, alternative fuels are investigated through LCCA, in which costs related to ship power systems are summed. Besides investment, fuel, and maintenance costs, the carbon tax is considered, taking the NZES from Figure 3. The LCCA results are compared in Figure 21.

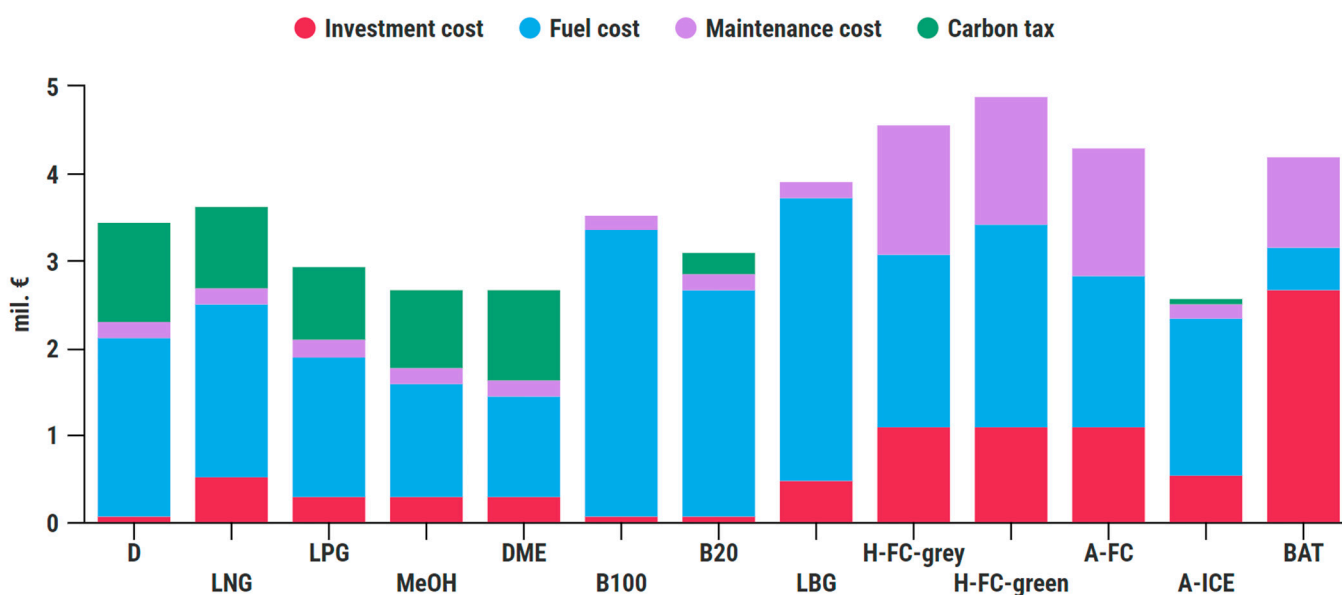


Figure 21. LCCA results.

The diesel-powered ship represents a baseline scenario, in which 60% of total costs refers to fuel cost. The most cost-efficient alternatives to replace diesel are DME, methanol, and ammonia used in dual-fuel engines. The most expensive alternatives are powering options that offer zero-emission shipping. High fuel costs and high costs related to the purchase of the main element of the system are the reasons why these alternative solutions are not currently profitable.

The LCA and LCCA comparison highlighted particular fuels as the most appropriate alternatives. They are presented in Table 6, where their reduction/increase in emissions and costs compared to the diesel-powered ship is indicated.

Table 6. Results of the replacement of the diesel-power system with highlighted alternatives.

	<i>GWP</i>	<i>AP</i>	<i>AFP</i>	Costs
H-FC-green	−88.4%	−84.5%	−90.5%	+29.7
A-ICE	+27.1%	−79.5%	−80.1%	−25.2%
DME	−2.3%	−79.3%	−79.3%	−22.0%
AES	−33.1%	−87.2%	−92.0%	+18.2%
B100	−87.1%	−0.3%	−0.6%	+2.8%
LPG	−24.4%	−90.7%	−90.7%	−15.0%
MeOH	−23.3%	−73.8%	−73.4%	−22.4%



According to the results presented in Table 6, green hydrogen in a fuel cell significantly reduces the environmental impact of the ship, but it increases its lifetime costs by 30%. Moreover, by omitting the carbon tax, the costs increase by 53%. Further development of fuel cell technology would lead to decreasing their costs, which would make fuel-cell-powered purse seiners a feasible powering solution. The LCCA highlighted the use of ammonia in ICE as the most cost-efficient option among those investigated, but the LCA comparison showed that this power system configuration increases the impact on climate change while reducing the impact on acidification and human toxicity.

Although battery power systems onboard Croatian ferries represent the most environmentally and economically appropriate alternative to conventional marine fuel, the full electrification of the Croatian purse seiner would result in higher costs than the existing powering option. The main reason for this is trip duration. Ferries operate frequently, follow schedules on fixed routes, and the onboard battery can be charged with shore power while passengers and vehicles are boarding. However, purse seiners cruise to the open sea and do not cruise back until the fishing trip is over, which can last over 10 h. Due to that, battery capacity needs to be enough to support the purse seiner in each fishing activity. The battery capacity of the considered ship is 4.8 MWh (weighted 22 tons), which results in major investment costs that make up 64% of the total costs. The all-electric ship results in a 40.2% lower carbon footprint than the existing ship. However, high investment and maintenance costs are limitations for the widespread use of fully electrified purse seiners.

The alternative solutions that satisfy both the environmental and economic criteria of the alternative fuel comparison are the LPG-powered ship and methanol-powered ship. Their use onboard reduces the environmental impact of the ship at a reasonable price. However, the use of LPG as marine fuel needs to be further developed and methanol is a more suitable alternative. The technology behind its use onboard is familiar and commercially available, and it has been implemented in many ship types. Although methanol use onboard cannot reach a GHG reduction of 50%, a hybrid power system with methanol in a dual-fuel engine and a battery can achieve the required reduction at reasonable costs.

In order to highlight the uncertainty regarding fuel prices, a sensitivity analysis was conducted, in which fuel prices varied by  $\pm 30\%$  with an increment of 10%. The analysis was performed for several fuels and the results are presented in Figure 22.

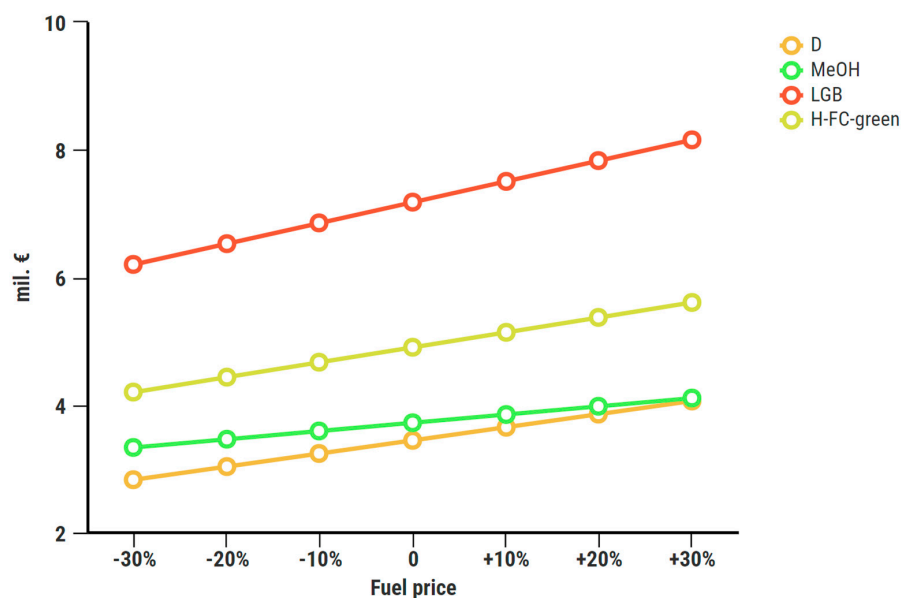


Figure 22. Sensitivity analysis.

The results presented in Figure 22 show that fuel price fluctuations can influence the total cost of a ship's power system. Among the investigated fuels, LGB is sensitive to fuel

price fluctuations, since more than 80% of the total costs related to ship power systems is fuel cost (due to great fuel consumption and high fuel price).

## 5. Conclusions

This paper considered the implementation of different alternative fuels onboard a Croatian purse seiner. The LCA investigated the environmental impact of fuel on three impact categories (climate change, acidification, and human toxicity), while the LCCA included investment, fuel, and maintenance costs, but also the carbon tax, which relates only to ship power systems with tailpipe emissions. The main findings of the research can be summarised as follows:

- The LCA indicated that the most environmentally friendly option is green hydrogen used in a fuel cell, while the second alternative with the lowest emissions compared to the diesel-powered ship is B100. On the other hand, the power systems with the highest released GHGs are LNG in a dual-fuel engine (due to methane slip), ammonia (in fuel cells and ICE), and the use of grey hydrogen in a fuel cell system.
- The LCAs that investigated the impact of alternative fuels on acidification and human toxicity indicated that the most environmentally friendly options are LPG and a fully electrified ship, while the greatest contributor is diesel, due to its high sulphur content.
- Although the LCA indicated that the use of green hydrogen results in the lowest emissions, the LCCA showed that its use in a fuel cell has the highest costs. The power system configurations that are cost-effective are ammonia in ICE, methanol, and DME.
- Methanol and LPG used in a dual-fuel engine were highlighted as the most appropriate fuels that satisfy environmental and economic criteria, i.e., their implementation achieves a reduction in emissions and cost compared to diesel-powered ships. A methanol power system results in a reduction in GHG and costs of 23.3% and 22.4%. Although LPG showed a higher reduction in GHG emissions (15.0%) at a reduced cost (24.4%), methanol is a more appropriate fuel for purse seiners. It has been thoroughly investigated as a marine fuel, and it is used in many types of ships.

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## Nomenclature

### Variables

<i>AFP</i>	aerosol formation potential (t PM 2.5 -eq)
<i>AP</i>	acidification potential (t SO <sub>2</sub> -eq)
<i>BC</i>	battery capacity (kWh)
<i>CA</i>	carbon allowance (EUR/t CO <sub>2</sub> )
<i>E</i>	emission (t)
<i>EC</i>	energy consumption (kWh)

<i>EF</i>	emission factor (g emission/kg)
<i>EH</i>	energy for heating of fuel cell system (kWh)
<i>FC</i>	fuel consumption (kg)
<i>GWP</i>	global warming potential (t CO <sub>2</sub> -eq)
<i>LHV</i>	lower heating value (MJ/kg)
<i>m</i>	weight of an engine/t)
<i>P</i>	power (kW)
<i>SFC</i>	specific fuel consumption (kg/kWh)
<i>t</i>	time (h)
<i>x</i>	share (%)
Subscripts	
A	annual
AE	auxiliary engine
ave	average
f	fuel
ME	main engine
p-f	pilot fuel
Greek letters	
$\eta$	efficiency (-)
Abbreviations	
AES	All-Electric Ship
A-FC	Ammonia in a Fuel Cell
A-ICE	Ammonia in an Internal Combustion Engine
APS	Announced Pledges Scenario
CII	Carbon Intensity Indicator
CNG	Compressed Natural Gas
D	Diesel
DME	Dimethyl-ether
ECA	Emission Control Area
EEDI	Energy Efficiency Design Index
EEXI	Energy Efficiency Existing Ship Index
ETS	Emission Trading System
FAO	Food and Agriculture Organisation
FU	Functional Unit
GHG	Greenhouse Gas
GT	Gross tonnage
H-FC	Hydrogen in fuel cell
HFO	Heavy Fuel Oil
ICE	Internal Combustion Engine
IES	Isolated Energy System
IMO	International Maritime Organisation
LBG	Liquefied Biogas
LCA	Life-Cycle Assessment
LCCA	Life-Cycle Cost Assessment
LNG	Liquefied Natural Gas
LPG	Liquefied Petroleum Gas
LSFO	Low-Sulphur Fuel Oil
M	Manufacturing
MDO	Marine Diesel Oil
MeOH	Methanol
NZES	Net Zero Emissions Scenario
PEMFC	Proton Exchange Membrane Fuel Cell
PM	Particulate Matter
RES	Renewable Energy Source
SEEMP	Ship Energy Efficiency Management Plan
SOFC	Solid Oxide Fuel Cell
SPS	Stated Policies Scenario
TTW	Tank-to-Wake
WTT	Well-to-Tank

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